

Permit Modification No. 1



IESI TIMBERLANE LANDFILL

D-003-8646 / P-0339
AI No. 52277

Oakdale, Louisiana

September 2007



10305 Airline Highway
Baton Rouge, Louisiana 70816

GRSA-SIGMA

CONSULTANTS AND ENGINEERS

Daniel B. Kais, P.E., President
 D. Todd Drummond, P.E., Vice President
 Stephen J. Brasuell, P.E., Director

Gary W. Cadby, Chief Executive Officer
 Corey E. Sullivan, Vice President
 Michael N. Dooley, M.B.A., P.E., Director

MAIN FILE

September 19, 2007

original to IOSW
 copy to SW/G3/Thomas
 AVG

PER20060001

Mr. Bijan Sharafkhani, P.E.
 Louisiana Department of Environmental Quality
 Office of Environmental Services
 P.O. Box 4313
 Baton Rouge, LA 70821-4313

Subject: Request for Final Copies
 Modification No. 7
 IESI Timberlane Landfill
 D-003-8646 P-0339 / AI 52277 ✓
 Oakdale, Louisiana (PER20060001)

Dear Mr. Sharafkhani:

Sigma Engineers and Constructor's (SEC), on behalf of IESI LA Landfill Corporation, is respectfully submitting six (6) final copies of modification no. 7 as requested.

If you have any questions concerning this submittal please contact Mr. Dale Steib, P.E. at (225) 298-0800 or Mr. Mike Friesen (817) 632-4246.

Very truly yours,

SIGMA ENGINEERS AND CONSTRUCTORS, INC.

Dale L. Steib, P.E.

C: Mike Friesen, IESI Corp.
 Marvin Kelch, IESI Timberlane Landfill

Attachments

RECEIVED
 SEP 20 2007

LDEQ



Permit Modification No. 7

IESI Timberlane Landfill

D-003-8646 / P-0339
AI No. 52277

Oakdale, Louisiana

September 2007

RECEIVED
SEP 20 2007
LDEQ

PART II

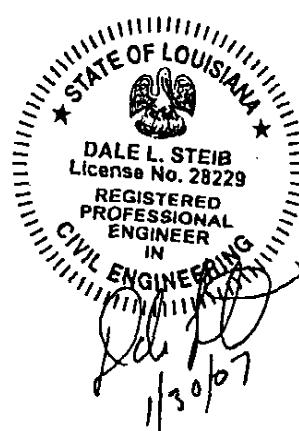
IESI TIMBERLANE LANDFILL

SIGMA ENGINEERS & CONSTRUCTORS, INC.

IESI Timberlane Landfill
Agency Interest Number - 52277
Facility Identification Number - D-003-8646
Permit Number - P-0339

"I certify under penalty of law that I have personally examined and I am familiar with the information submitted in this permit application modification and that the facility as described in this permit application meets the requirements of the Solid Waste Rules and Regulations. I am aware that there are significant penalties for knowingly submitting false information, including the possibility of fine and imprisonment."

DALE L. STEIB, P.E.
LA. REG. NO. 28229



RECEIVED
SEP 20 2007
LDEQ

Permit Modification No.7
January 2007

IESI Timberlane Landfill
Agency Interest Number - 52277
Facility Identification Number - D-003-8646
Permit Number - P-0339

LAC 33:VII.521.F.3.a.

3. The following information on plans and specifications is required for Type I, II, and III landfills:

- a. approximate dimensions of daily fill and cover; and

RESPONSE:

Timberlane Landfill will utilize silty clays and sandy clays for daily cover as well as any other LDEQ approved material. As each day's disposal area approaches final grades, daily cover will be applied so that at the end of the work day, all waste has a minimum of six (6") inches of soil cover or is covered by the manufacturer's recommended thickness of an LDEQ approved Material. After the landfill has been in operation and the disposal areas are well defined, a portable synthetic cover such as tarps or plastic sheets may also be utilized as a substitute for daily cover. However, if synthetic covers are used under no conditions shall waste go more than three (3) days without a 6" soil cover being placed. An interim cover (12 inches) or interim compacted cover (24 inches) composed of similar soil types as the daily cover will be applied in lifts of six (6") inches compacted thickness within 48 hours of the last receipt of solid waste in an operating area and on all operating areas not receiving solid waste for a period longer than 60 days.

The exact width and depth of the daily cover applied will vary according to the amount of waste received each particular day. However, ideal depth varies between 10 and 15 feet with a standard disposal area width between 100 and 150 feet.

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The installation of daily and interim cover at the facility will help to minimize vector-breeding and animal attraction, control leachate generation, reduce fire-hazard potential, minimize blowing paper and litter, reduce noxious odors, provide an aesthetic appearance and allow accessibility regardless of weather.

Alternate forms of daily cover may be used including but not limited to hydro mulching such as "waste-Cover" and "Posi-Shell". The specifications, MSDS sheet and operational plans for these hydro mulching products are given in Appendix 45. These materials satisfy all the requirements specified in accordance with LAC 711.B.2.a as reflected in the manufacturers published documentation. Another application of hydro mulch, or another LDEQ approved material or 6" of soil will be applied to areas that will not receive waste for more than seven days.

The approved alternate daily cover manufacturers' operation plan and/or application procedures will be followed.

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LAC 33:VII.521.F.4.c.

c. a description of the leachate collection and removal system, which shall include calculations of anticipated leachate volumes, rationale for particular designs of such systems, and drawings.

RESPONSE:

Timberlane Landfill will implement a leachate system which collects and treats leachate generated at the site. The leachate collection system will utilize a pipe network strategically placed on top of the disposal area's composite liner system. This pipe network will consist of a series of 6 inch perforated pipes running parallel to each other in collection trenches with a maximum overland flow distance of 100 feet (See Exhibit 9 for plans and Exhibits 13 - 16 for details). The collection trenches will be 24 inches wide by 10 inches deep, shaped in the form of a "V" and filled with gravel and wrapped by a geotextile fabric in contact with the walls of the trench and double lapped across the top.
(See detail on Exhibit 13)

Leachate from the disposal area will migrate through a 12 inch leachate collection layer of granular matter having a permeability of 1×10^{-2} cm/sec or a geonet drainage layer overlain by a 12" protective cover material with the minimum permeability of 1×10^{-4} cm/sec located on top of the disposal area's composite liner. From that point, the collected leachate will travel towards the perimeter of the disposal area, via leachate collection pipes at a minimum 1% slope to collection sumps.

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LAC 33:VII.521.J.1.a.

J. Facility Closure. Standards governing facility closure are contained in LAC 33:VII.711.E (Type I and II landfills), LAC 33:VII.713.E (Type I and II surface impoundments), LAC 33:VII.715.E (Type I and II landfarms), LAC 33:VII.717.I (Type I-A and II-A facilities), LAC 33:VII.721.D (construction and demolition debris and woodwaste landfills), LAC 33:VII.723.D (Type III composting facilities), and LAC 33:VII.725.D (Type III separation facilities)

1. The closure plan for all facilities must include the following:
 - a. the date of final closure;

RESPONSE:

The acceptance of solid waste at Timberlane Landfill began in August 2003. Based on estimated waste volumes of 50,000 cubic gate yards a month with an annual increase of approximately—approximately 53%, the date of final closure for Area I of the facility is projected to be in the year of 2013~~2021~~, which translates into 11-17 years of life.(See Appendix 44)

Available air space volumes at the facility were derived from the information found in Appendix No. 35 and are estimated at approximately 9.06—9.45 million cubic yards in place. Landfill life calculations were based on the estimated average monthly waste volume received at the facility of 50,000 cubic gate yards with a 35% growth factor and a compaction factor of 2.

At least 90 days prior to the closure, sealing or abandonment of any unit at the facility, written notification will be given to the administrative authority indicating the date of planned closure, changes requested in the approved closure plan, closure schedule or estimated cost.

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LAC 33:VII.521.J.2.a.

2. The closure plan for Type I and II landfills and surface impoundments must include:

a. a description of the final cover and the methods and procedures used to install the cover;

RESPONSE:

After final machine compacting and grading have occurred and a disposal area is ready for closure, a final cap will be installed. This final cap will consist of 24 inches of recompacted clay with a permeability of less than 1×10^{-7} cm/sec, a ~~40 mil FML~~ and topped with a minimum of 6 inches of top soil capable of supporting vegetation. This final cap will be installed in accordance with the Minimum Quality Control/Accurance Procedures for Clay Bottom and Cap Liner Installation found in Appendix No. 31, Construction Quality Assurance for Synthetic Bottom and Cap Liner Installation found in Appendix No. 32, and minimum Construction Quality Assurance Procedures for Top Soil installation found in Appendix No. 25. Prior to installation of the ~~40 mil FML~~ and the top soil, the gas collection system will be installed. Currently there are no slopes less steep than a 4:1 with the current permitted design but if there are any slopes less steep than 4:1 at closure then a HDPE layer will be included on those slopes. 180 days prior to closure IESI will submit a revised closure plan which will reflect the required changes needed if any.

The 1% slopes at the stormwater diversion berms will incorporate an HDPE liner at the path of water conveyance. (see exhibit 15, for detail)

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LAC 33:VII.521.J.2.c.

c. an estimate of the maximum inventory of solid waste ever on-site over the active life of the facility; and

RESPONSE:

Waste will be disposed of on a daily basis, thus no waste will be stored at Timberlane Landfill. The estimated volume of waste to be disposed of is 9.069.45 million cubic yards of in place waste. Using a compaction factor of 2.0 results in approximately 18.1218.90 million cubic yards of gate volume.

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LAC 33:VII.521.J.2.d.

d. a schedule for completing all activities necessary for closure.

RESPONSE:

It is anticipated that Area I of the Timberlane Landfill will have an anticipated life of 43 17 years. Assuming that no additional expansion is approved, closure of the landfill would begin approximately 43–17 years after the initial operation of the facility.

Construction of the final phase of the gas collection system, synthetic cap and recompacted clay liner for the landfill should take one calendar year from last receipt of waste.

The post closure period will be a minimum of 30 years during which time the oxidation pond will most probably remain in use. Once the oxidation pond is no longer needed, the pond will be dewatered and clean closed. This closure will take approximately two years to complete. This date will be approximately 45 years after the landfill first received waste.

APPENDIX 35
ESTIMATED LANDFILL QUANITITIES

Timberlane Total volume

Site Volume Table: Unadjusted

Cut cu.yds	Fill cu.yds	Net cu.yds	Method
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Site: 60610 Timberlane

Stratum: total permitted landfill volume entire top pc layer bottom of final cover

0	9445497	9445497 (F) Composite
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Cell 1 Under Cut Area at Floor

$$5.2417 \text{ acres} = 288,330 \text{ sq.ft} \times 3 \text{ ft.} = 684,990 \text{ cu.ft} = 25,370 \text{ cu.yds}$$

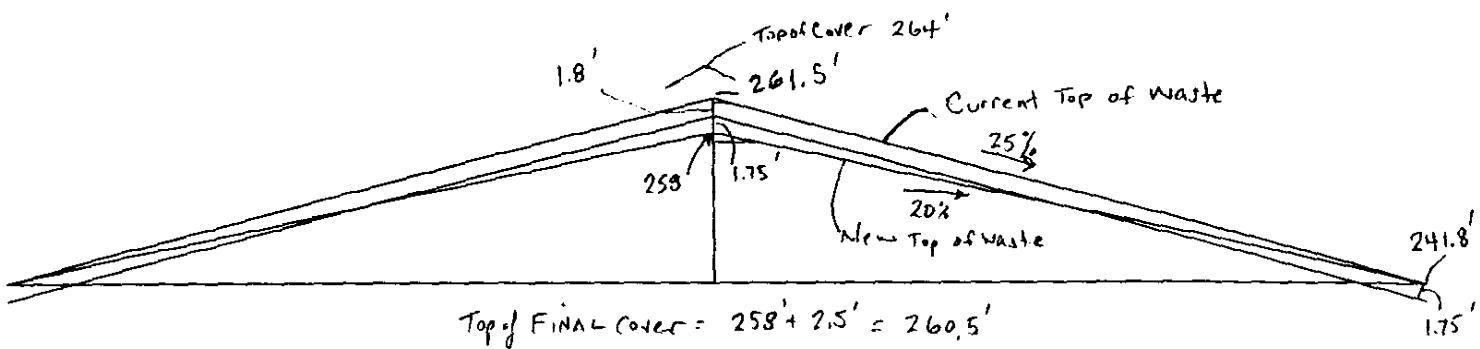
Final Cover Reduction

Based on Areas of Final cap at Elevation 241.8'

$$\text{Area} = 380,550 \text{ sq.ft} \times 1.8 \text{ ft.} = 684,990 \text{ cu.ft} = 25,370 \text{ cu.yds}$$

On Final Cover every Contour at and above Elevation 241.8' is lowered by 1.8 feet.
 This reduces the

Final Contour Slope above elevation 241.2 from a 25% slope to a 20% slope.



APPENDIX 38
HELP MODEL CALCULATIONS

IESI TIMBERLANE LANDFILL

SIGMA ENGINEERS & CONSTRUCTORS, INC.

TIMBNFML

WARNING: TEMPERATURE FOR YEAR 1 USED WITH PRECIPITATION FOR YEAR 1974

WARNING: SOLAR RADIATION FOR YEAR 1 USED WITH PRECIPITATION FOR YEAR 1974

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*****
***** HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE *****
***** HELP MODEL VERSION 3.01 (14 OCTOBER 1994) *****
***** DEVELOPED BY ENVIRONMENTAL LABORATORY *****
***** USAE WATERWAYS EXPERIMENT STATION *****
***** FOR USEPA RISK REDUCTION ENGINEERING LABORATORY *****
*****
```

PRECIPITATION DATA FILE: C:\HELPMO-1\timb.D4
 TEMPERATURE DATA FILE: C:\HELPMO-1\timb.D7
 SOLAR RADIATION DATA FILE: C:\HELPMO-1\timb.D13
 EVAPOTRANSPIRATION DATA: C:\HELPMO-1\timb.D11
 SOIL AND DESIGN DATA FILE: C:\HELPMO-1\timbnfml.D10
 OUTPUT DATA FILE: C:\HELPMO-1\timbnfml.OUT

*New Run without the
FML on Top.
Used Same parameters
for comparison*

TIME: 19:50 DATE: 2/22/2007

No Applicative Difference

TITLE: Timberlane Landfill 25% Final Cover Slope (No FML)

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 13

THICKNESS	=	6.00 INCHES
POROSITY	=	0.4300 VOL/VOL
FIELD CAPACITY	=	0.3210 VOL/VOL
WILTING POINT	=	0.2210 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.3837 VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.33000003000E-04 CM/SEC

NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00
FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

TIMBNFML

LAYER 2

TYPE 3 - BARRIER SOIL LINER
MATERIAL TEXTURE NUMBER 16

THICKNESS	=	24.00	INCHES
POROSITY	=	0.4270	VOL/VOL
FIELD CAPACITY	=	0.4180	VOL/VOL
WILTING POINT	=	0.3670	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.4270	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.10000001000E-06	CM/SEC

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 18

THICKNESS	=	1800.00	INCHES
POROSITY	=	0.6710	VOL/VOL
FIELD CAPACITY	=	0.2920	VOL/VOL
WILTING POINT	=	0.0770	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2920	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000005000E-02	CM/SEC

LAYER 4

TYPE 2 - LATERAL DRAINAGE LAYER
MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.4170	VOL/VOL
FIELD CAPACITY	=	0.0450	VOL/VOL
WILTING POINT	=	0.0180	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0450	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.989999995000E-02	CM/SEC
SLOPE	=	0.00	PERCENT
DRAINAGE LENGTH	=	0.0	FEET

LAYER 5

TYPE 4 - FLEXIBLE MEMBRANE LINER
MATERIAL TEXTURE NUMBER 35

THICKNESS	=	0.06	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.199999996000E-12	CM/SEC
FML PINHOLE DENSITY	=	4.00	HOLES/ACRE

TIMBNFML

FML INSTALLATION DEFECTS	=	0.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	4 - POOR	

LAYER 6

TYPE 3 - BARRIER SOIL LINER
MATERIAL TEXTURE NUMBER 16

THICKNESS	=	36.00	INCHES
POROSITY	=	0.4270	VOL/VOL
FIELD CAPACITY	=	0.4180	VOL/VOL
WILTING POINT	=	0.3670	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.4270	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000001000E-06	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS USER-SPECIFIED.

SCS RUNOFF CURVE NUMBER	=	74.00	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	71.000	ACRES
EVAPORATIVE ZONE DEPTH	=	6.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	2.302	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	2.580	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	1.326	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	554.062	INCHES
TOTAL INITIAL WATER	=	554.062	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
Lake Charles LOUISIANA

MAXIMUM LEAF AREA INDEX	=	2.00	
START OF GROWING SEASON (JULIAN DATE)	=	32	
END OF GROWING SEASON (JULIAN DATE)	=	361	
AVERAGE ANNUAL WIND SPEED	=	8.70	MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY	=	77.00	%
AVERAGE 2ND QUARTER RELATIVE HUMIDITY	=	77.00	%
AVERAGE 3RD QUARTER RELATIVE HUMIDITY	=	80.00	%
AVERAGE 4TH QUARTER RELATIVE HUMIDITY	=	78.00	%

NOTE: PRECIPITATION DATA FOR LAKE CHARLES LOUISIANA
WAS ENTERED FROM THE DEFAULT DATA FILE.

TIMBNFML

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR SHREVEPORT LOUISIANA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
54.50	54.30	60.70	68.40	74.90	80.40
82.30	81.60	78.20	69.30	59.70	53.90

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR LAKE CHARLES LOUISIANA

STATION LATITUDE = 30.10 DEGREES

WARNING: TEMPERATURE FOR YEAR 1 USED WITH PRECIPITATION FOR YEAR 1974

WARNING: SOLAR RADIATION FOR YEAR 1 USED WITH PRECIPITATION FOR YEAR 1974

ANNUAL TOTALS FOR YEAR 1974

	INCHES	CU. FEET	PERCENT
PRECIPITATION	66.44	17123580.000	100.00
RUNOFF	40.981	10562113.000	61.68
EVAPOTRANSPIRATION	24.215	6240907.000	36.45
PERC./LEAKAGE THROUGH LAYER 2	1.243771	320557.094	1.87
AVG. HEAD ON TOP OF LAYER 2	3.2787		
DRAINAGE COLLECTED FROM LAYER 4	1.2438	320557.094	1.87
PERC./LEAKAGE THROUGH LAYER 6	0.000000	0.000	0.00
AVG. HEAD ON TOP OF LAYER 6	0.0011		
CHANGE IN WATER STORAGE	0.000	0.000	0.00
SOIL WATER AT START OF YEAR	554.062	142798416.000	
SOIL WATER AT END OF YEAR	554.062	142798416.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	3.349	0.00

TIMBNFML

WARNING: TEMPERATURE FOR YEAR 2 USED WITH PRECIPITATION FOR YEAR 1975

WARNING: SOLAR RADIATION FOR YEAR 2 USED WITH PRECIPITATION FOR YEAR 1975

ANNUAL TOTALS FOR YEAR 1975

	INCHES	CU. FEET	PERCENT
PRECIPITATION	55.51	14306591.000	100.00
RUNOFF	27.251	7023522.000	49.09
EVAPOTRANSPIRATION	26.766	6898429.500	48.22
PERC./LEAKAGE THROUGH LAYER 2	1.316162	339214.562	2.37
AVG. HEAD ON TOP OF LAYER 2	3.1992		
DRAINAGE COLLECTED FROM LAYER 4	1.3162	339214.562	2.37
PERC./LEAKAGE THROUGH LAYER 6	0.000000	0.000	0.00
AVG. HEAD ON TOP OF LAYER 6	0.0012		
CHANGE IN WATER STORAGE	0.176	45429.945	0.32
SOIL WATER AT START OF YEAR	554.062	142798416.000	
SOIL WATER AT END OF YEAR	554.238	142843840.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	-5.008	0.00

WARNING: TEMPERATURE FOR YEAR 3 USED WITH PRECIPITATION FOR YEAR 1976

WARNING: SOLAR RADIATION FOR YEAR 3 USED WITH PRECIPITATION FOR YEAR 1976

ANNUAL TOTALS FOR YEAR 1976

	INCHES	CU. FEET	PERCENT
PRECIPITATION	40.40	10412289.000	100.00

	TIM8NFM		
RUNOFF	16.596	4277213.500	41.08
EVAPOTRANSPIRATION	22.746	5862396.500	56.30
PERC./LEAKAGE THROUGH LAYER 2	1.176277	303161.781	2.91
Avg. HEAD ON TOP OF LAYER 2	2.7153		
DRAINAGE COLLECTED FROM LAYER 4	1.1763	303161.812	2.91
PERC./LEAKAGE THROUGH LAYER 6	0.000000	0.000	0.00
Avg. HEAD ON TOP OF LAYER 6	0.0011		
CHANGE IN WATER STORAGE	-0.118	-30485.885	-0.29
SOIL WATER AT START OF YEAR	554.238	142843840.000	
SOIL WATER AT END OF YEAR	554.120	142813360.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	3.533	0.00

WARNING: TEMPERATURE FOR YEAR 4 USED WITH PRECIPITATION FOR YEAR 1977

WARNING: SOLAR RADIATION FOR YEAR 4 USED WITH PRECIPITATION FOR YEAR 1977

ANNUAL TOTALS FOR YEAR 1977

	INCHES	CU. FEET	PERCENT
PRECIPITATION	57.37	14785965.000	100.00
RUNOFF	31.852	8209188.500	55.52
EVAPOTRANSPIRATION	24.150	6224097.000	42.09
PERC./LEAKAGE THROUGH LAYER 2	1.196101	308271.187	2.08
Avg. HEAD ON TOP OF LAYER 2	2.9346		
DRAINAGE COLLECTED FROM LAYER 4	1.1961	308271.156	2.08
PERC./LEAKAGE THROUGH LAYER 6	0.000000	0.000	0.00
Avg. HEAD ON TOP OF LAYER 6	0.0011		
CHANGE IN WATER STORAGE	0.172	44407.457	0.30
SOIL WATER AT START OF YEAR	554.120	142813360.000	

	TIMBNFML		
SOIL WATER AT END OF YEAR	554.292	142857776.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	0.737	0.00

WARNING: TEMPERATURE FOR YEAR 5 USED WITH PRECIPITATION FOR YEAR 1978

WARNING: SOLAR RADIATION FOR YEAR 5 USED WITH PRECIPITATION FOR YEAR 1978

ANNUAL TOTALS FOR YEAR 1978

	INCHES	CU. FEET	PERCENT
PRECIPITATION	41.44	10680330.000	100.00
RUNOFF	22.001	5670327.000	53.09
EVAPOTRANSPIRATION	18.669	4811652.500	45.05
PERC./LEAKAGE THROUGH LAYER 2	0.977150	251840.969	2.36
AVG. HEAD ON TOP OF LAYER 2	2.4568		
DRAINAGE COLLECTED FROM LAYER 4	0.9772	251841.000	2.36
PERC./LEAKAGE THROUGH LAYER 6	0.000000	0.000	0.00
AVG. HEAD ON TOP OF LAYER 6	0.0009		
CHANGE IN WATER STORAGE	-0.208	-53484.008	-0.50
SOIL WATER AT START OF YEAR	554.292	142857776.000	
SOIL WATER AT END OF YEAR	554.085	142804288.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	-6.529	0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1974 THROUGH 1978

TIMBNFML

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	6.40 3.84	2.09 5.91	2.46 4.58	3.63 3.39	4.49 5.54	5.60 4.32
STD. DEVIATIONS	3.89 2.20	1.12 3.64	0.67 1.17	2.98 2.12	4.43 1.48	1.69 2.76
RUNOFF						
TOTALS	4.689 1.315	0.955 3.388	0.292 2.489	1.740 1.581	2.246 3.342	2.928 2.770
STD. DEVIATIONS	3.842 1.574	0.868 2.869	0.551 1.396	1.937 1.301	3.221 1.302	1.641 2.870
EVAPOTRANSPIRATION						
TOTALS	1.559 2.339	1.687 2.300	1.821 2.426	2.089 1.353	1.870 1.712	2.645 1.508
STD. DEVIATIONS	0.112 0.732	0.110 0.941	0.363 0.266	0.562 0.806	1.015 0.410	0.614 0.170
PERCOLATION/LEAKAGE THROUGH LAYER 2						
TOTALS	0.1256 0.0857	0.1073 0.0838	0.0953 0.1124	0.0919 0.0757	0.0755 0.1059	0.0999 0.1228
STD. DEVIATIONS	0.0057 0.0367	0.0087 0.0487	0.0150 0.0086	0.0223 0.0399	0.0504 0.0179	0.0290 0.0066
LATERAL DRAINAGE COLLECTED FROM LAYER 4						
TOTALS	0.1256 0.0857	0.1073 0.0838	0.0953 0.1124	0.0919 0.0757	0.0755 0.1059	0.0999 0.1228
STD. DEVIATIONS	0.0057 0.0367	0.0087 0.0487	0.0150 0.0086	0.0223 0.0399	0.0504 0.0179	0.0290 0.0066
PERCOLATION/LEAKAGE THROUGH LAYER 6						
TOTALS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000
STD. DEVIATIONS	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)**DAILY AVERAGE HEAD ACROSS LAYER 2**

AVERAGES	4.7336 2.3968	3.7743 2.3475	1.9098 3.3488	1.8745 2.0169	1.9640 3.5125	2.8966 4.2278
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	TIMBNFML					
STD. DEVIATIONS	1.0040	0.8335	0.3485	0.8212	1.6724	0.9114
	1.7598	1.6649	0.8385	1.3571	1.1619	1.0532
DAILY AVERAGE HEAD ACROSS LAYER 6						
AVERAGES	0.0014	0.0013	0.0010	0.0010	0.0008	0.0011
	0.0009	0.0009	0.0013	0.0008	0.0012	0.0013
STD. DEVIATIONS	0.0001	0.0001	0.0002	0.0002	0.0005	0.0003
	0.0004	0.0005	0.0001	0.0004	0.0002	0.0001

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1974 THROUGH 1978

	INCHES	CU. FEET	PERCENT
PRECIPITATION	52.23 (11.130)	13461750.0	100.00
RUNOFF	27.736 (9.3489)	7148473.00	53.102
EVAPOTRANSPIRATION	23.309 (2.9716)	6007496.00	44.626
PERCOLATION/LEAKAGE THROUGH FROM LAYER 2	1.18189 (0.12650)	304609.125	2.26278
AVERAGE HEAD ACROSS TOP OF LAYER 2	2.917 (0.340)		
LATERAL DRAINAGE COLLECTED FROM LAYER 4	1.18189 (0.12650)	304609.125	2.26278
PERCOLATION/LEAKAGE THROUGH FROM LAYER 6	0.00000 (0.00000)	0.000	0.00000
AVERAGE HEAD ACROSS TOP OF LAYER 6	0.001 (0.000)		
CHANGE IN WATER STORAGE	0.005 (0.1715)	1173.50	0.009

PEAK DAILY VALUES FOR YEARS 1974 THROUGH 1978

	(INCHES)	(CU. FT.)
PRECIPITATION	5.88	1515452.370
RUNOFF	5.867	1512075.6200
PERCOLATION/LEAKAGE THROUGH LAYER 2	0.004252	1095.84412
AVERAGE HEAD ACROSS LAYER 2	6.000	

	TMBNFM	
DRAINAGE COLLECTED FROM LAYER 4	0.00425	1095.84412
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.000000	0.00000
AVERAGE HEAD ACROSS LAYER 6	0.001	
SNOW WATER	1.83	471727.1250
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4300
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2020

0

FINAL WATER STORAGE AT END OF YEAR 1978

LAYER	(INCHES)	(VOL/VOL)
1	2.3249	0.3875
2	10.2480	0.4270
3	525.6000	0.2920
4	0.5400	0.0450
5	0.0000	0.0000
6	15.3720	0.4270
SNOW WATER	0.000	

APPENDIX NO. 38

HELP CALCULATIONS

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** HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE  

** HELP MODEL VERSION 3.04 (13 MARCH 1995)  

** DEVELOPED BY ENVIRONMENTAL LABORATORY  

** USACE WATERWAYS EXPERIMENT STATION  

** FOR USEPA RISK REDUCTION ENGINEERING LABORATORY  

**  

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PRECIPITATION DATA FILE: C:\HELP3\TIBERLN\TINPREC.D4
 TEMPERATURE DATA FILE: C:\HELP3\TIBERLN\TINTEMP.D7
 SOLAR RADIATION DATA FILE: C:\HELP3\TIBERLN\TINSOLR.D13
 EVAPOTRANSPIRATION DATA: C:\HELP3\TIBERLN\TINBEVAP.D11
 SOIL AND DESIGN DATA FILE: C:\HELP3\TIBERLN\TINSOIL.D10
 OUTPUT DATA FILE: C:\HELP3\TIBERLN\TINOUT.OUT

*Original Run
 for Permit
 Application*

TIME: 10:42 DATE: 1/ 8/1997

 TITLE: TIMBERLAKE LANDFILL

 NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SHOW WATER WERE
 COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 13

THICKNESS	=	6.00 INCHES
POROSITY	=	0.4300 VOL/VOL
FIELD CAPACITY	=	0.3210 VOL/VOL
WILTING POINT	=	0.2210 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.3922 VOL/VOL
EFFECTIVE SAT. WT. COND.	=	0.330000003000E-04 CM/SEC

NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00
 FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

THICKNESS	=	0.06 INCHES
POROSITY	=	0.0000 VOL/VOL
FIELD CAPACITY	=	0.0000 VOL/VOL
WILTING POINT	=	0.0000 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000 VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.199999996000E-12 CU/SEC
FML PINHOLE DENSITY	=	4.00 MOLES/ACRE
FML INSTALLATION DEFECTS	=	0.00 MOLES/ACRE
FML PLACEMENT QUALITY	=	4 - POOR

LAYER 3

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

THICKNESS	=	24.00 INCHES
POROSITY	=	0.4270 VOL/VOL
FIELD CAPACITY	=	0.4180 VOL/VOL
WILTING POINT	=	0.3670 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.4270 VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.10000001000E-06 CU/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 18

THICKNESS	=	1800.00 INCHES
POROSITY	=	0.6710 VOL/VOL
FIELD CAPACITY	=	0.2920 VOL/VOL
WILTING POINT	=	0.0770 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2920 VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.10000005000E-02 CU/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 1

THICKNESS	=	12.00 INCHES
POROSITY	=	0.4170 VOL/VOL
FIELD CAPACITY	=	0.0450 VOL/VOL
WILTING POINT	=	0.0180 VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0451 VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.99999978000E-02 CU/SEC

SLOPE	=	2.00	PERCENT
DRAINAGE LENGTH	=	100.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 35

THICKNESS	=	0.06	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.199999996000E-12	CM/SEC
FAL PINHOLE DENSITY	=	4.00	MOLES/ACRE
FAL INSTALLATION DEFECTS	=	0.00	MOLES/ACRE
FAL PLACEMENT QUALITY	=	4 - POOR	

LAYER 7

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 16

THICKNESS	=	36.00	INCHES
POROSITY	=	0.4270	VOL/VOL
FIELD CAPACITY	=	0.4180	VOL/VOL
WILTING POINT	=	0.3670	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.4270	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.10000001000E-06	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS USER-SPECIFIED.

SCS RUNOFF CURVE NUMBER	=	76.00	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	71.000	ACRES
EVAPORATIVE ZONE DEPTH	=	6.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	2.353	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	2.580	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	1.326	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	554.114	INCHES
TOTAL INITIAL WATER	=	554.114	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
LAKE CHARLES LOUISIANA

STATION LATITUDE	= 30.10 DEGREES
MAXIMUM LEAF AREA INDEX	= 2.00
START OF GROWING SEASON (JULIAN DATE)	= 32
END OF GROWING SEASON (JULIAN DATE)	= 361
EVAPORATIVE ZONE DEPTH	= 6.0 INCHES
AVERAGE ANNUAL WIND SPEED	= 8.70 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY	= 77.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY	= 77.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY	= 80.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY	= 78.00 %

NOTE: PRECIPITATION DATA FOR LAKE CHARLES LOUISIANA
WAS ENTERED FROM THE DEFAULT DATA FILE.

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR LAKE CHARLES LOUISIANA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
.....
51.50	56.30	60.70	68.40	74.90	80.40
82.30	81.60	78.20	69.30	59.70	53.90

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR LAKE CHARLES LOUISIANA
AND STATION LATITUDE = 30.10 DEGREES

MONTHLY TOTALS (IN INCHES) FOR YEAR 1974

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
.....
PRECIPITATION	12.69	3.89	3.37	2.95	11.01	2.89
	1.28	5.54	3.60	4.15	7.30	7.77
RUNOFF	10.981	2.066	1.530	0.966	5.358	0.272
	0.000	1.468	1.722	2.274	4.180	5.894
EVAPOTRANSPIRATION	1.687	2.327	1.851	2.460	4.414	3.872

	1.210	3.341	2.677	0.860	2.947	2.029
PERCOLATION/LEAKAGE THROUGH LAYER 3	0.0012	0.0008	0.0003	0.0002	0.0003	0.0002
	0.0009	0.0003	0.0005	0.0002	0.0010	0.0011
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.0010	0.0009	0.0007	0.0005	0.0003	0.0003
	0.0002	0.0001	0.0004	0.0003	0.0005	0.0008
PERCOLATION/LEAKAGE THROUGH LAYER 7	0.0009	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

MONTHLY SUMMARIES FOR DAILY HEADS (INCHES)

AVERAGE DAILY HEAD ON TOP OF LAYER 2	5.529	4.021	1.446	1.082	1.454	1.008
	0.000	1.234	2.469	0.853	4.695	5.045
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 2	0.443	0.944	1.909	1.738	1.509	1.411
	0.000	2.068	1.998	1.547	0.923	0.651
AVERAGE DAILY HEAD ON TOP OF LAYER 6	0.003	0.003	0.002	0.001	0.001	0.001
	0.000	0.000	0.001	0.001	0.002	0.002
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 6	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

ANNUAL TOTALS FOR YEAR 1976

	INCHES	CU. FEET	PERCENT
	-----	-----	-----
PRECIPITATION	66.44	17123580.000	100.00
RUNOFF	36.752	9472036.000	55.32
EVAPOTRANSPIRATION	29.676	7648404.000	44.67
PERC./LEAKAGE THROUGH LAYER 3	0.006049	1558.896	0.01
AVG. HEAD ON TOP OF LAYER 2	2.4031		
DRAINKAGE COLLECTED FROM LAYER 5	0.0060	1555.920	0.01
PERC./LEAKAGE THROUGH LAYER 7	0.000010	2.647	0.00
AVG. HEAD ON TOP OF LAYER 6	0.0015		
CHANGE IN WATER STORAGE	0.006	1573.059	0.01
SOIL WATER AT START OF YEAR	554.114	142811854.000	
SOIL WATER AT END OF YEAR	554.120	142813424.000	

ANNUAL TOTALS FOR YEAR 1975

	INCHES	CU. FEET	PERCENT
PRECIPITATION	55.51	16306591.000	100.00
RUNOFF	19.693	5075570.500	35.48
EVAPOTRANSPIRATION	35.632	9183337.000	64.19
PERC./LEAKAGE THROUGH LAYER 3	0.005424	1397.863	0.01
Avg. HEAD ON TOP OF LAYER 2	2.1124		
DRAINAGE COLLECTED FROM LAYER 5	0.0059	1514.461	0.01
PERC./LEAKAGE THROUGH LAYER 7	0.000010	2.616	0.00
Avg. HEAD ON TOP OF LAYER 6	0.0014		
CHANGE IN WATER STORAGE	0.179	46169.285	0.32
SOIL WATER AT START OF YEAR	554.120	142813424.000	
SOIL WATER AT END OF YEAR	554.299	142859600.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANUAL WATER BUDGET BALANCE	0.0000	-3.008	0.00

MONTHLY TOTALS (IN INCHES) FOR YEAR 1976

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION	2.10 2.72	1.48 0.77	2.53 3.26	1.22 4.51	2.43 3.16	7.50 6.72
RUNOFF	0.557 0.000	0.447 0.000	0.000 0.000	0.000 2.139	0.000 2.797	3.517 5.274
EVAPOTRANSPIRATION	1.634 3.473	2.008 0.687	2.168 2.342	1.395 2.301	2.040 2.304	3.942 1.628

PERCOLATION/LEAKAGE THROUGH LAYER 3	0.0008	0.0005	0.0002	0.0001	0.0001	0.0003
	0.0001	0.0000	0.0003	0.0005	0.0006	0.0011
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.0006	0.0006	0.0004	0.0003	0.0002	0.0002
	0.0002	0.0001	0.0001	0.0003	0.0005	0.0008
PERCOLATION/LEAKAGE THROUGH LAYER 7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

MONTHLY SUMMARIES FOR DAILY HEADS (INCHES)

AVERAGE DAILY HEAD ON TOP OF LAYER 2	3.706	2.683	1.054	0.481	0.402	1.589
	0.403	0.000	1.383	2.354	3.836	5.093
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 2	1.268	1.640	1.475	0.589	0.780	2.055
	0.753	0.000	1.711	1.600	1.542	0.710
AVERAGE DAILY HEAD ON TOP OF LAYER 6	0.002	0.002	0.001	0.001	0.001	0.001
	0.001	0.000	0.000	0.001	0.002	0.002
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 6	0.892	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

ANNUAL TOTALS FOR YEAR 1976

	INCHES	CU. FEET	PERCENT
-----	-----	-----	-----
PRECIPITATION	40.40	10412289.000	100.00
RUNOFF	14.730	3796467.250	36.46
EVAPOTRANSPIRATION	25.920	6680420.500	64.16
PERC./LEAKAGE THROUGH LAYER 3	0.004931	1270.892	0.01
Avg. HEAD ON TOP OF LAYER 2	1.9154		
DRAINAGE COLLECTED FROM LAYER 5	0.0065	1151.795	0.01
PERC./LEAKAGE THROUGH LAYER 7	0.000008	2.172	0.00
Avg. HEAD ON TOP OF LAYER 6	0.0011		
CHANGE IN WATER STORAGE	-0.255	-65738.141	-0.63
SOIL WATER AT START OF YEAR	554.299	142859600.000	
SOIL WATER AT END OF YEAR	554.044	142793856.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00

BLOW WATER AT END OF YEAR	\$ 0.000	0.000	\$ 0.00
AVERAGE WATER BUDGET BALANCE	-0.0001	-14,237	\$ 0.00

MONTHLY TOTALS (IN INCHES) FOR YEAR 1977

MONTHLY SUMMARIES FOR DAILY MEADS (INCHES)

ANNUAL TOTALS FOR YEAR 1977

	INCHES	CU. FEET	PERCENT
PRECIPITATION	57.37	14785963.000	100.00
RUNOFF	20.182	7263454.000	49.12
EVAPOTRANSPIRATION	28.932	7456684.500	50.43
PERC./LEAKAGE THROUGH LAYER 3	0.005536	1626.863	0.01
Avg. Head on top of Layer 2	2.1697		
DRAINKAGE COLLECTED FROM LAYER 5	0.0058	1493.733	0.01
PERC./LEAKAGE THROUGH LAYER 7	0.000010	2.576	0.00
Avg. Head on top of Layer 6	0.0014		
CHANGE IN WATER STORAGE	0.250	64322.387	0.44
SOIL WATER AT START OF YEAR	554.044	142793856.000	
SOIL WATER AT END OF YEAR	554.294	142858176.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00
ANNUAL WATER BUDGET BALANCE	0.0000	7.929	0.00

MONTHLY TOTALS (IN INCHES) FOR YEAR 1978

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION	6.28 5.02	2.45 7.24	1.48 6.04	0.52 0.18	0.34 4.14	6.00 1.75
RUNOFF	6.842 1.124	0.865 4.510	0.003 3.164	0.000 0.000	0.000 1.388	2.643 0.000
EVAPOTRANSPIRATION	1.653 3.358	2.129 2.355	1.416 3.574	1.028 0.353	0.340 1.691	3.356 2.031
PERCOLATION/LEAKAGE THROUGH LAYER 3	0.0011 0.0002	0.0009 0.0001	0.0002 0.0006	0.0000 0.0000	0.0000 0.0003	0.0003 0.0005

LATERAL DRAINKAGE COLLECTED FROM LAYER 5	0.0008	0.0009	0.0007	0.0006	0.0001	0.0002
	0.0001	0.0002	0.0003	0.0003	0.0002	0.0004
PERCOLATION/LEAKAGE THROUGH LAYER 7	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

MONTHLY SUMMARIES FOR DAILY HEADS (INCHES)

AVERAGE DAILY HEAD ON TOP OF LAYER 2	5.221	4.605	1.030	0.194	0.000	1.182
	1.078	0.485	2.958	0.060	1.460	2.447
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 2	0.698	1.153	1.614	0.444	0.000	1.739
	1.766	1.273	1.302	0.202	1.497	1.726
AVERAGE DAILY HEAD ON TOP OF LAYER 6	0.002	0.003	0.002	0.001	0.000	0.001
	0.000	0.001	0.001	0.001	0.001	0.001
STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 6	0.000	0.000	0.000	0.000	0.000	0.000
	0.000	0.000	0.000	0.000	0.000	0.000

ANNUAL TOTALS FOR YEAR 1978

	INCHES	CU. FEET	PERCENT

PRECIPITATION	41.44	10680330.000	100.00
RUNOFF	18.519	4772867.000	44.69
EVAPOTRANSPIRATION	23.283	6000778.500	56.19
PERC./LEAKAGE THROUGH LAYER 3	0.004360	1123.776	0.01
Avg. HEAD ON TOP OF LAYER 2	1.7268		
DRAINKAGE COLLECTED FROM LAYER 5	0.0047	1199.104	0.01
PERC./LEAKAGE THROUGH LAYER 7	0.000009	2.221	0.00
Avg. HEAD ON TOP OF LAYER 6	0.0011		
CHANGE IN WATER STORAGE	-0.367	-94525.117	-0.89
SOIL WATER AT START OF YEAR	554.294	142558176.000	
SOIL WATER AT END OF YEAR	553.927	142763648.000	
SNOW WATER AT START OF YEAR	0.000	0.000	0.00
SNOW WATER AT END OF YEAR	0.000	0.000	0.00

ANNUAL WATER BUDGET BALANCE 0.0000 7,964 0.00

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1974 THROUGH 1978

	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
STD. DEVIATIONS	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

AVERAGES OF MONTHLY AVERAGED DAILY READS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 2

AVERAGES	4.7940	3.3263	1.3166	0.8315	0.7327	1.1499
	0.8020	1.1408	2.5160	1.5846	2.8746	3.7187
STD. DEVIATIONS	0.7475	0.9289	0.2751	0.4795	0.8134	0.3257
	0.8048	0.8931	0.9662	1.1286	1.3534	1.3362

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	0.0025	0.0025	0.0017	0.0011	0.0007	0.0007
	0.0006	0.0006	0.0011	0.0010	0.0013	0.0018
STD. DEVIATIONS	0.0005	0.0004	0.0003	0.0002	0.0003	0.0002
	0.0003	0.0004	0.0005	0.0004	0.0004	0.0006

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1976 THROUGH 1978

	INCHES	CU. FEET	PERCENT
PRECIPITATION	52.23 (11.130)	13461750.0	100.00
RUNOFF	23.575 (8.8560)	6076079.00	45.136
EVAPOTRANSPIRATION	20.689 (4.6401)	7393925.50	54.925
PERCOLATION/LEAKAGE THROUGH LAYER 3	0.00526 (0.00064)	1355.658	0.01007
AVERAGE HEAD ON TOP OF LAYER 2	2.065 (0.257)		
LATERAL DRAINAGE COLLECTED FROM LAYER 3	0.00537 (0.00074)	1383.003	0.01027
PERCOLATION/LEAKAGE THROUGH LAYER 7	0.00001 (0.00000)	2.446	0.00002
AVERAGE HEAD ON TOP OF LAYER 6	0.001 (0.000)		
CHANGE IN WATER STORAGE	-0.037 (-0.2679)	-9639.71	-0.072

PEAK DAILY VALUES FOR YEARS 1974 THROUGH 1978

	(INCHES)	(CU. FT.)
PRECIPITATION	5.88	1515452.370
RUNOFF	5.842	1505666.8700
PERCOLATION/LEAKAGE THROUGH LAYER 3	0.000040	10.41500
AVERAGE HEAD ON TOP OF LAYER 2	6.000	
DRAINKAGE COLLECTED FROM LAYER 5	0.00003	8.95251
PERCOLATION/LEAKAGE THROUGH LAYER 7	0.000000	0.01265
AVERAGE HEAD ON TOP OF LAYER 6	8.003	
MAXIMUM HEAD ON TOP OF LAYER 6	0.192	
SNOW WATER	1.83	471727.1250
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.4300
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.2210

*** MAXIMUM HEADS ARE COMPUTED USING THE HOUND EQUATION. ***

FINAL WATER STORAGE AT END OF YEAR 1978

LAYER	(INCHES)	(VOL/VOL)
1	2.1668	0.3611
2	0.0000	0.0000
3	10.2480	0.4270
4	525.6000	0.2920
5	0.5404	0.0450
6	0.0000	0.0000
7	15.3720	0.4270
SNOW WATER	0.000	

APPENDIX 44

SITE LIFE TABLE

TABLE 1
TIMBERLANE LANDFILL SITE LIFE CALCULATION

Total Available Volume (cubic yards)	Current Volume (cubic yards)	Remaining Volume (cubic yards)	% Filled	Remaining Life (Years)
Original Permit Area	9,445,497	0	9,445,497	0.0%
	Disposed cubic yards for that year	total in place cubic yards	cubic yards per day that year	No. years
2004	432,530	432,530	1,512	
2005	432,530	865,060	1,512	1
2006	454,157	1,319,217	1,588	2
2007	476,864	1,796,081	1,667	3
2008	500,708	2,296,788	1,751	4
2009	525,743	2,822,531	1,838	5
2010	552,030	3,374,561	1,930	6
2011	579,632	3,954,193	2,027	7
2012	608,613	4,562,806	2,128	8
2013	639,044	5,201,850	2,234	9
2014	670,996	5,872,846	2,346	10
2015	704,546	6,577,392	2,463	11
2016	739,773	7,317,165	2,587	12
2017	776,762	8,093,926	2,716	13
2018	815,600	8,909,526	2,852	14
2019	856,380	9,765,906	2,994	15
2020	899,199	10,665,105	3,144	16
2021	944,159	11,609,264	3,301	17

Assumptions:

286 days a year
5.5 days a week
980 tpd (initially)
5.0% per year growth rate
waste density = 48pcf

Conversion Calculation:

980 ton/day x 1/48 ft³/lbs x 2000 lbs/ton x 1/27 cy/ft³ = 2314.8 cy/day x 52 week x 5.5 day/week = 432,530 cy/year

APPENDIX 45
ALTERNATE DAILY COVER SPECIFICATIONS

IESI TIMBERLANE LANDFILL

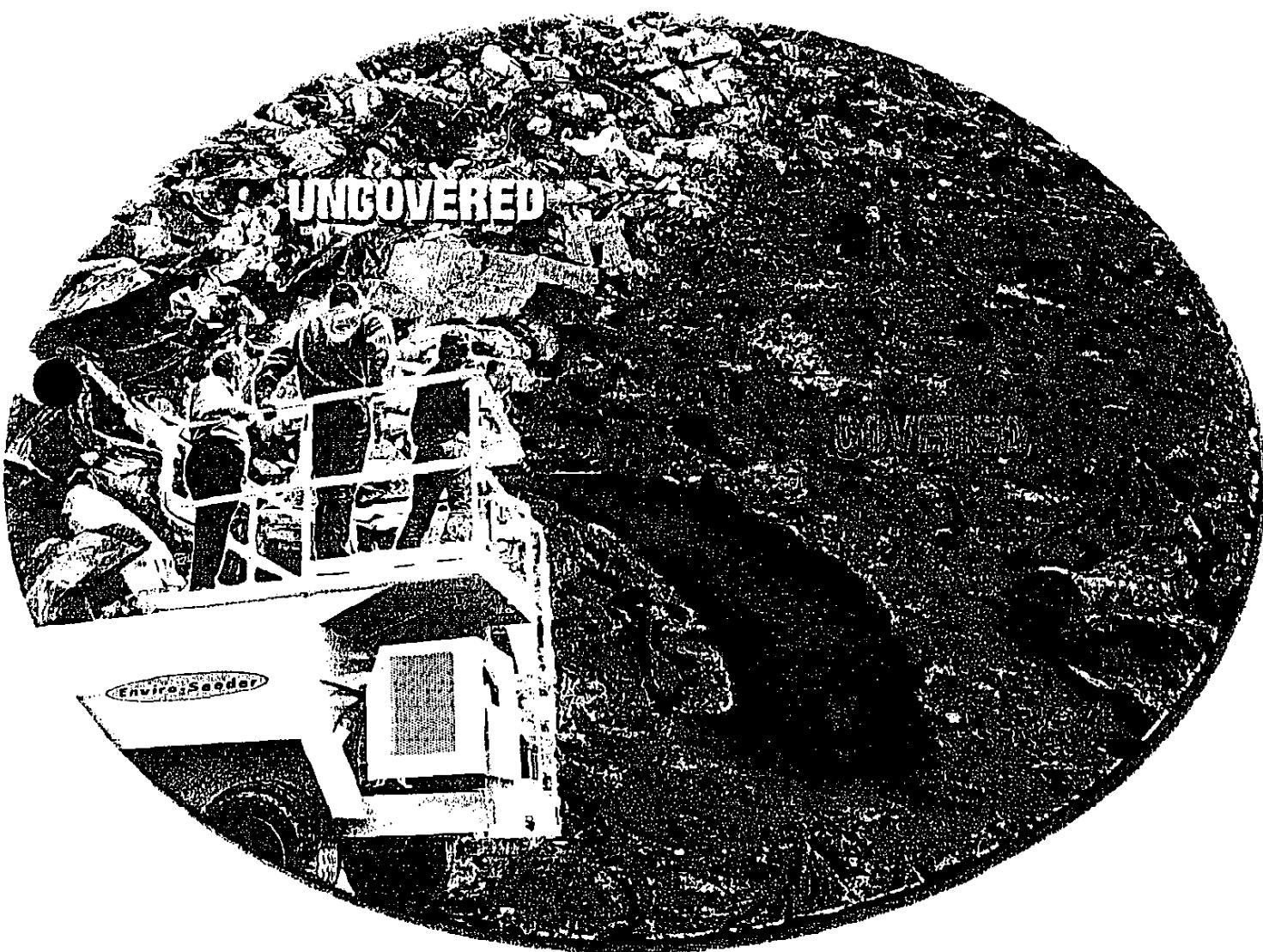
SIGMA ENGINEERS & CONSTRUCTORS, INC.



WASTE-COVER

DAILY LANDFILL COVER

By the year 2009, four of five landfills will be full!



SOUTHWEST ENVIRONMENT SERVICES, INC.

2400 E. ERWIN • P.O. BOX 134 • TYLER, TEXAS 75702

903/531-2211 • FAX 903/531-2312

Web Site - www.southwestenvironment.com

"A Leader in Erosion Control"

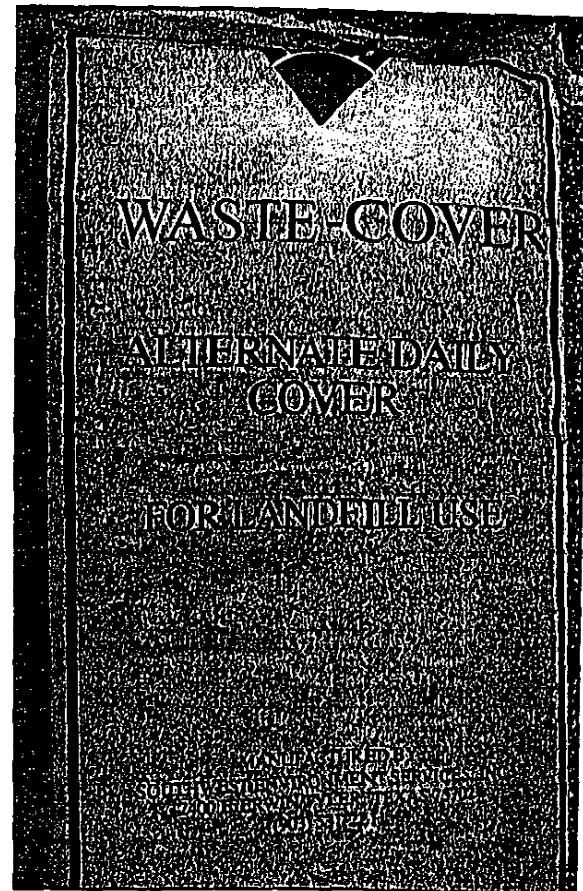
WASTE-COVER

WASTE-COVER is an alternate daily landfill cover manufactured from recycled paper and wood polymers, enzyme complex, and other proprietary ingredients. Waste-Cover helps breakdown the garbage faster and helps alleviate odors. All ingredients are non-toxic and biodegradable. Lend Mother Nature a helping hand, make your landfill more efficient by using Waste-Cover.

- ▼ Meets ASTM D6523-ADC
- ▼ Easy to mix
- ▼ Sprays easily
- ▼ Non-flammable
- ▼ Controls blowing litter
- ▼ Controls odor and disease vector
- ▼ Aesthetically acceptable
- ▼ Repels vermin
- ▼ One dry component, eliminates fine powders and dust
- ▼ Use conventional hydraulic mulching machines

Mix Ratio & Coverage Data

Mix ratio: 1 bag to
60 gallons water
Coverage (1 bag): 450 sq. ft. per bag



Application and Coverage Data

Tank	Amount Water	Pounds of Waste-Cover	Number of Bags	Coverage Sq.Ft.
500 gal.	420 gal.	350 lbs.	7	3150 sq. ft.
700 gal.	540 gal.	450 lbs.	9	4050 sq. ft.
900 gal.	780 gal.	650 lbs.	13	5850 sq. ft.
100 gal.	900 gal.	750 lbs.	15	6750 sq. ft.
1200 gal.	1020 gal.	850 lbs.	17	7650 sq. ft.
1500 gal.	1380 gal.	1150 lbs.	23	10350 sq. ft.



MATERIAL SAFETY DATA SHEET

Identify: **WASTE COVER**
(Alternate Daily Cover)

I. General Information

Manufacturer's Name:	Southwest Environmental Services
Address:	2400 East Erwin, Tyler, Texas 75702
Telephone Number:	(903) 531-2211
HMIS Rating:	Health - 0 (normal material) Fire - 1 (flash point above 200°F) Reactivity - 0 (stable)

II. Hazardous Ingredients

Component:	Paper/Wood Mulch (as fibers) 67-68 % by wt
CAS:	9004-34-6 (as fibers), non-hazardous material except for potential of air-borne fibers.
OSHA PEL:	For fibers/dust - 15 mg/m ³ (total), 5 mg/m ³ (respirable)
Component:	Binder (non-specific) 30 % by wt
CAS:	26499-65-0
OSHA PEL:	For dust - 15 mg/m ³ (total), 5 mg/m ³ (respirable)
Component:	Ammonium sulfate 2 % by wt
CAS:	7783-20-2
OSHA PEL:	For dust - 15 mg/m ³ (total), 5 mg/m ³ (respirable)

Remaining Ingredients Constitute Less Than (<) 1 % of Product Material.

III. Physical Characteristics

Appearance:	Mulched solid, tan, grayish-green
Odor:	No discernible, characteristic odor
Density:	0.97 g/cm ³
pH:	6.2
Solubility (in water):	Insoluble; will disperse in water
Melting/Boiling Point:	Not applicable
Reactivity in Water:	Non-reactive



IV. Fire and Explosion Hazard Data

Flash Point: Greater than ($>$) 200°F
Combustibility: Non-combustible at standard temperature and pressure, difficult to ignite.
Extinguishing Media: Water/Foam
Fire Fighting Procedures: Routine
Special Procedures: None

V. Reactivity

Stability: Stable
Compatibility: For product integrity avoid excessive moisture or humidity until ready for use.
Conditions to Avoid: None
Hazardous Polymerization: Will not occur
Hazardous Decomposition: None except those produced from typical combustion of normal materials (CO₂, CO).

VI. Health Hazard Data

Route(s) of Entry: Inhalation (as dust/fibers), incidental ingestion, dermal/eye contact.
Primary route of Exposure: Inhalation (as dust)
Effects of Overexposure: Inhalation - mildly toxic as an acute irritant to mucus membranes and upper respiratory system.
Carcinogenicity: None
Aggravated Conditions: Respiratory disorders or diseases may be aggravated by exposure from dust/fibers
Emergency/First Aid: Inhalation - remove from exposure (remove to fresh air). If not breathing, give artificial respiration. If breathing is difficult, give oxygen. Consult a physician.
 Ingestion - None required for slight ingestion. For large ingested quantity, induce vomiting. Consult a physician.
 Dermal/Eye Contact - Wash material from skin using soap and water. In case of eye contact, flush eyes with water.



VII. Safe Handling and Use

- Storage:** Maintain in original sealed containers provided by manufacturer. Material should be stored in a manner to prevent accumulations of airborne dust. Avoid excessive moisture/humidity to insure product integrity. Sweep/remove excess material and containerize.
- Releases or Spills:**
- Waste Disposal Method:** This material, as a waste and as provided by the manufacturer, is not a federally-defined hazardous waste (40 CFR 261). Dispose of in accordance with applicable Federal/State/Local requirements.

VIII. Special Protection/Control Measures

- Respiratory Protection:** Respiratory protection required if OSHA PEL (dust) is exceeded. Use of a standard pollen/dust type mask is recommended as a precautionary measure.
- Ventilation:** Normal ventilation is usually adequate to maintain exposure levels below OSHA PEL. Respiratory protection is required if allowable exposure level is exceeded.
- Eye Protection:** The use of goggles and/or safety glasses are recommended as a precautionary measure.
- Skin Protection:** The use of gloves is recommended as a precautionary measure if skin is broken or sensitive.
- Work/Hygienic Practices:** Clean and properly operating personal protective equipment (PPE) when required. No other PPE recommended or required. Use standard hygienic practices as with most non-hazardous materials.

Date Prepared: 4/16/02

Prepared by:

Steven R. Kennedy, C.E.T., REM
PTTL Engineers & Consultants Inc.
Tyler, Texas
(903) 595-4421

Page 3 of 3 - MSDS - Waste Cover



PROCEDURE FOR APPLYING HYDROMULCH AS AN ALTERNATIVE DAILY COVER

TRAINING

The operators shall be familiar with the M.S.D.S. for all hydromulch material. Training will be conducted on the use of the material and the operations of the hydroseeder to properly apply the hydromulch.

MIXING PROCEDURE

The operator will mix the fiber material into the appropriate amount of water. Upon the addition of all bags of fiber, the total batch will be agitated at about half speed for a minimum of 15 minutes before application. The correct amount of all ingredients will be determined by the supplier. The total amount of the hydromulch to be applied is directly proportional to the size (square feet) of the active work face and the extent of the compaction of the surface. For each 900 square feet of active work face, the following amounts should be used:

Water	120 gallons
Waste-Cover	100 lbs.

APPLICATION PROCEDURE

The application of a hydromulch mixture should be done to the entire working face of the landfill at the end of the workday. This is best accomplished by directing the flow of hydromulch into the air allowing it to "rain down" onto the active working face. This will ensure that no shadows are created as a result of inadequate surface compaction. The operator may elect to apply the mulch from two directions to ensure that all areas are covered and all shadowing is eliminated. Complete coverage is required to meet LAC 33:V11.711.B.2. for controlling disease vectors, fire, odors, vermin, blowing litter, scavenging and creating an acceptable aesthetes. The hydromulch mixture must be applied to a thickness of 1/4" or greater. This can be done from the tower of a standard hydroseeding machine.

If inclement weather conditions render the placement of hydromulch as a daily cover ineffective, the landfill shall temporarily revert to using another approved daily cover such as tarps or 6" of dirt.

The mixture of Waste-Cover is non-toxic, non-combustible, totally biodegradable, and harmless to fish, birds, plants, and animals.

Operation Plan:

- Fiber mulch mix will be applied as daily cover on well compacted exposed waste
- Materials will be mixed and applied to the entire active working face in accordance with the manufacturer's specification
- The application will be made at the end of each work day
- The hydromulch mixture will be applied with a landfill modified hydroseeder to a thickness of 1/4" or greater
- The hydromulch applied as a slurry should be allowed to dry for approx. 2 hours depending on weather conditions
- Traffic will be restricted over the areas covered until the material has set.
- Hydromulch can be applied in moderate rain. During heavy inclement weather, other approved material will be used for daily cover
- Each application should last for seven days, after which additional waste must be added to the working face or another application of hydromulch could be performed

Based on local D.E.Q. requirements

PROCEDURE FOR APPLYING HYDROMULCH AS AN ALTERNATIVE DAILY COVER

TRAINING

The operators shall be familiar with the M.S.D.S. for all hydromulch material. Training will be conducted on the use of the material and the operations of the hydroseeder to properly apply the hydromulch.

MIXING PROCEDURE

The operator will mix the fiber material into the appropriate amount of water. Upon the addition of all bags of fiber, the binder will be added last and the total batch will be agitated at about half speed for a minimum of 15 minutes before application. The correct amount of all ingredients will be determined by the supplier. The total amount of the hydromulch to be applied is directly proportional to the size (square feet) of the active work face and the extent of the compaction of the surface. For each 900 square feet of active work face, the following amounts should be used:

1-Water	100 to 110 gallons
2-Waste-Cover	100 lbs. (2 Bags)

APPLICATION PROCEDURE

The application of a hydromulch mixture should be done to the entire working face of the landfill at the end of the workday. This is best accomplished by directing the flow of hydromulch into the air allowing it to rain down onto the active working face. This will ensure that no shadows are created as a result of inadequate surface compaction. The operator may elect to apply the mulch from two directions to ensure that all areas are covered and all shadowing is eliminated. Complete coverage is required to meet LAC 33:V11.711.B.2. for controlling disease vectors, fire, odors, vermin, blowing litter, scavenging and creating an acceptable aesthetes. The hydromulch mixture must be applied to a thickness of $\frac{1}{4}$ " or greater. This can be done from the tower of a standard hydroseeding machine.

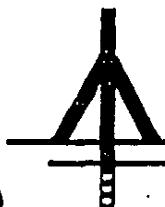
If inclement weather conditions render the placement of hydromulch as a daily cover ineffective, the landfill shall temporarily revert to using another approved daily cover such as tarps or 6" of dirt.

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- Traffic will be restricted over the areas covered until the material has dried
- Hydromulch can be applied in moderate rain. During heavy inclement weather, other approved material will be used for daily cover
- Each application should last for seven days¹, after which additional waste must be added to the working face or another application of hydromulch could be performed

¹Based on local D.E.Q. requirements



STE
Soil Testing Engineers, Inc.

318 HIGHLANDIA DRIVE (70810) • P.O. BOX 63710 (70884) • BATON ROUGE, LOUISIANA
PHONE (225) 752-4790 • FAX (225) 752-4878 • www.steola.com

GORDON P. BOUTWELL, JR., Ph.D.
CHING N. TSAI, Ph.D.
DANIEL J. HOLDER, MS
CHAD M. POCHE, MS
CHARLES S. HEDGES, MS
KENNETH A. FLUKER, MS
ZIAO H. ALEM, MS
STEVE M. MEUNIER
KELLIE T. McNAMARA

November 21, 2001

Louisiana Vegetation
Post Office Box 33812
Baton Rouge, Louisiana 70884

Attn: Mr. Don Breaux

Re: Alternative Daily Cover
Flammability Potential
STE File: 01-3044

Gentlemen:

We have completed the Flammability Potential Screening Analysis of Waste (ASTM D4982-95) on a sample of WASTE COVER submitted by Mr. Andrew St. Pierre on November 21, 2001. Method A of the above procedure was performed on the sample submitted. Following Section 9 (Procedure) of Method A the sample was found to have a negative Flammability Potential.

If you have any questions concerning this information, please contact us at 225-752-4790.

Sincerely,
Soil Testing Engineers, Inc.

A handwritten signature in black ink, appearing to read 'C.N.Tsai'.

Chung-Nien Tsai, Ph.D., P.E.
Chief Engineer

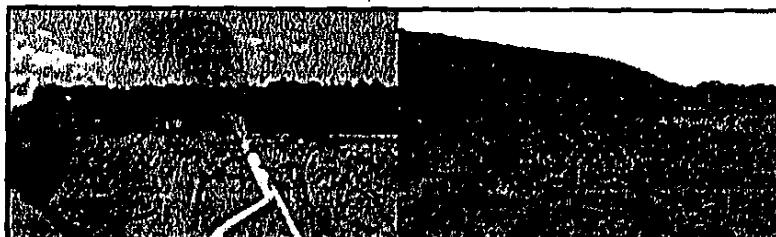
A handwritten signature in black ink, appearing to read 'G.L.Perkins'.

George L. Perkins, C.E.T.
QC Manager

GLP/kab

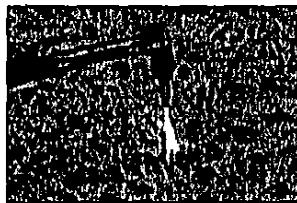
Posi-Shell Description

Page 1 of 2

**Description**

Posi-Shell Cover is a spray-applied, cement-mortar coating, similar to stucco, used for landfill daily cover, intermediate cover, erosion prevention, and odor control.

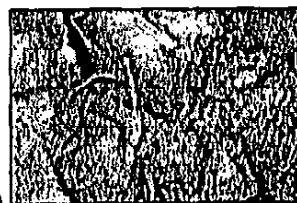
Posi-Shell replaces costly, and sometimes scarce soil as daily cover of landfill solid waste, thereby preserving a valuable natural resource, as well as conserving valuable air space, and greatly extending the life of a landfill.



Simple to mix and easy to use, the Posi-Shell Cover System consists of a liquid base, a mineral binder, and specialized Posi-Pak fibers. Because it forms a durable, non-flammable crust that resists wind and water erosion, Posi-Shell is also ideal for applications such as erosion control, ditch-lining, dust control, cover for contaminated soil, compost, coal, or cement clinker piles, mining applications, voc suppression, sludge tar lagoons, and similar industrial purposes.

POSI-SHELL ADVANCED FORMULATION

The Posi-Shell Advanced Formulation (AF) Cover System is a low-cost, versatile alternative to traditional landfill daily cover materials and is the ideal solution for both small and large landfills and industrial projects. It offers the same non-flammable durability as the traditional formulation of Posi-Shell, but our unique setting agent comes in bags for easy mixing and storage, plus it can be applied with common hydro-seeding equipment.



Posi-Shell AF is a spray-on slurry composed of water, Posi-Pak Type P-100 Fibers, PSM-200™ Setting Agent, and optionally, Portland cement. Like the traditional formulation of Posi-Shell, the Advanced Formulation hardens to a stucco-like cover that meets and exceeds regulatory requirements for the control of landfill vectors, fires, odors, blowing litter, and scavenging.

Posi-Shell Description

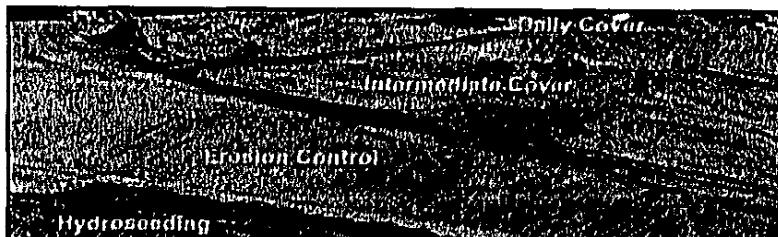
Page 2 of 2

Main Office
2183 Pennsylvania Avenue
Apalachin, NY 13732 USA

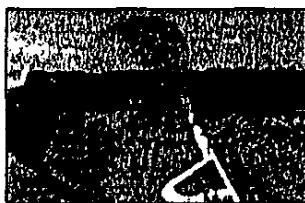
1 800 800 7671
Phone: 607 625 3050
Fax: 607 625 2689

Posi-Shell Applications - DAILY, INTERMEDIATE, AND LONG-TERM COVER

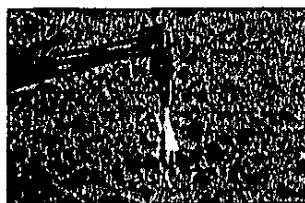
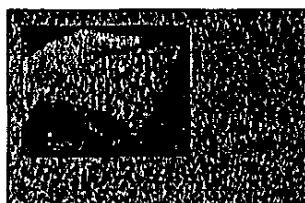
Page 1 of 2

**DAILY, INTERMEDIATE, AND LONG-TERM COVER**

Posi-Shell has been approved for daily cover, and intermediate and long-term cover for landfills, stockpiles, and hazardous waste sites. The primary component of the formulation is a cementitious mineral binder reinforced with structural composite fibers, which results in excellent resistance to erosion and cracking and provides long-term durability in various weather conditions.



Applying Posi-Shell cover is a simple one-person operation using either the specialized Posi-Shell equipment with the traditional Posi-Shell formulation, or a standard hydroseeding unit and Posi-Shell Advanced Formulation. One load of Posi-Shell requires just one hour for mixing, application, and rinse-out. Landfill operators realize a huge savings in airspace, labor, machinery, and fuel costs through use of the Posi-Shell Cover System over traditional soil cover.



After application, the Posi-Shell slurry hardens to a non-flammable and highly impermeable coating that easily conforms to the irregular contours of a landfill. Its color and texture provide a uniform appearance that is aesthetically appealing to nearby residents; and because of its inherent alkalinity, Posi-Shell suppresses typical landfill odors as well.



Posi-Shell is highly effective in preventing wind-blown litter, landfill fires, scavenging, and vector problems. Posi-Shell has met the rigorous standards required for approval by numerous state regulatory agencies and has been favorably

Posi-Shell Applications - DAILY, INTERMEDIATE, AND LONG-TERM COVER

Page 2 of 2

evaluated for Superfund use by the USEPA. Made of non-flammable, non-toxic materials, Posi-Shell is an environmentally compatible, multi-purpose landfill cover solution.

Posi-Shell Cover System:

- Conserves airspace
- Mitigates odors
- Reduces airborne debris
- Controls vector populations
- Enhances safety through non-flammability
- Discourages scavenging
- Cuts operating expenses
- Extends landfill life
- Increases profits

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2183 Pennsylvania Avenue
Apalachin, NY 13732 USA

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Fax: 607 625 2689



BRIEF SPECIFICATIONS

- Spray applied mortar containing greater than 50% by weight, cementitious mineral binder
- Fiber reinforced mixture incorporating quarter-inch very fine (1.5 ± 0.2) denier polyester fibers with proprietary finish for rapid, non-clumping, aqueous dispersal
- Non-combustible, non-fuel contributing, and non-smoke releasing in accordance with ASTM 1354
- No free liquid in accordance with paint filter test (negative result for SW-846)
- Hydraulic conductivity not greater than 1×10^{-5} cm/sec when cured
- Non-toxic as indicated by TCLP testing
- Self-contained diesel/hydraulic mineral binder storage silo with 50 ton Portland Cement capacity, capable of feeding 1 ton per minute into mixer-applicator
- Self-contained diesel/hydraulic towable mixer-applicator with 2000 gallon minimum slurry capacity capable of mixing load within 10 minutes. Progressing cavity mortar pump able to shoot mortar slurry 150 ft @ 100 GPM



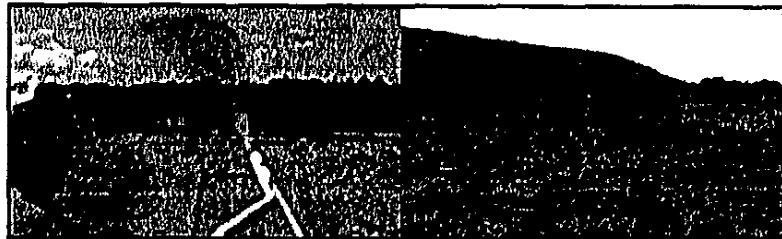
ADVANCED FORMULATION

BRIEF SPECIFICATIONS

- Spray applied mortar containing approximately 25% by weight, cementitious mineral materials
- Excellent opacity and adhesion to heterogeneous waste materials
- Fiber reinforced mixture incorporating quarter-inch very fine (1.5 ± 0.2) denier polyester fibers with proprietary finish for rapid, non-clumping, aqueous dispersal
- Complies with ASTM D6523 "Evaluation and Selection of Alternate Daily Covers (ADC) for Sanitary Landfills"
- Non-flammable in accordance with ASTM D4982 "Flammability Potential Screening Analysis for Waste"
- No free liquid in accordance with paint filter test (negative result for SW-846)
- Non-toxic as indicated by TCLP testing
- Can be applied with commonly available hydroseeding equipment, or with specialized landfill ADC machines

Posishell Coverage

Page 1 of 1



Application Coverage Rates

Category	Standard	Enhanced	Superior
Soil			
Leachate			
Water			
Waste			
Vegetation			
Structures			
Equipment			
Other			

Main Office
2183 Pennsylvania Avenue
Apalachin, NY 13732 USA

1 800 800 7671
Phone: 607 625 3050
Fax: 607 625 2689



American Standards Testing Bureau, Inc.

40 WATER STREET, NEW YORK, N.Y. 10004

PHONE: (212) 643-3184

FAX: (212) 646-2260

July 20, 1995

Landfill Service Corporation
2183 Pennsylvania Avenue
Apolachin, NY 13732

Att: Mr. George Nealon

Gentlemen:

RE: Heat & Visible Smoke Release Rates for Posi-Shell
ASTB P. #1235-536; LR. #29007

Pursuant to your recent request, ASTB/New York received and tested the heat and visible smoke release rates for one (1) Posi-Shell Cover System product as per the requirements of ASTM E-1354. The nominal heat fluxes were 25, 35 and 50 kW/m², respectively, and all specimens were tested in the horizontal orientation.

The Posi-Shell sample tested did not ignite at 25, 35 or 50 kW/m². At the most extreme heat flux, 50 kW/m², the mass loss of the specimen was 8.9%, although little or no smoke was observed. The measured peak and average values of the heat and visible smoke release rates at 50 kW/m² are:

<u>PEAK AND AVERAGE VALUES (50 kW/m²)</u>	<u>PEAK</u>	<u>TIME</u>	<u>AVERAGE</u>
Heat Release Rate (kW/m ²)	6.9	167	3.6
Eff. Heat of Comb. (MJ/kg)	827.8	512	2.7
Specific Ext. Area (m ² /kg)	4.2	17	0.4
CO (kg/kg)	0.0	600	0.0
CO ₂ (kg/kg)	0.8	380	0.0

Since ignition did not occur, the heat release rate, total heat released and effective heat of combustion are not considered to be useful data but are reported for completeness. In summary, the Posi-Shell examined must be classified as non-combustible, non-fuel contributing and non-smoke releasing material.

Respectfully submitted,

AMERICAN STANDARDS TESTING BUREAU, INC.

J.C. Brooks
S. C. Brooks, P.E.
Project Engineer

V. Marfopoulos
V. Marfopoulos, Eng.Sc.D.
Technical Director

SCB/VM/dk
Enc.



SOIL & MATERIAL TESTING, INC.

57 SOUTH MAIN STREET • CASTLETON, N.Y. 12033

Office	Telephone	Office	Telephone
Castleton	(518) 732-7205	Binghamton	(607) 722-1582
Fax	(518) 732-4516	Kingston	(914) 336-4471
		Pittsfield	(413) 499-5332

HYDRAULIC CONDUCTIVITY TEST DATA

Project Name: LANDFILL SERVICE CORP. POSI-SHELL

Client: Landfill Technologies, Inc.
PO Box 519
West Sand Lake, New York 12196

SMT Project No. 80799

Sample Description: Visual Description:
Gray Cementitious Material
Sample #1
Undisturbed Shelby Tube Specimen:

Date Sampled: 10/23/95
Date Reported: 10/31/95

Date Tested: 10/27/95
Reviewed By: REV *RW*

Test Standard: ASTM D 5084
Test By: DW

Test Description: Falling Head/Rising
tail Flexible Wall Permeability

RESULTS:

Initial Specimen Properties

Length = 8.20 cm
Diameter = 7.21 cm
Moisture Content = 63.0%
Wet Density = 96.5pcf
Dry Density = 59.2pcf

Test Conditions

Back Pressure = 66.0 psi
Cell Pressure = 70.0 psi
Hydraulic Gradient = 10
Permeant Liquid: Air-less
Tap Water

Remarks:

Hydraulic Conductivity: $k_{20} = 1.5 \times 10^{-6}$ cm/sec

SOIL & MATERIAL TESTING, INC.

Thomas M. Kenney
Thomas M. Kenney



SOIL & MATERIAL TESTING, INC.

57 SOUTH MAIN STREET • CASTLETON, N.Y. 12033

Office	Telephone	Office	Telephone
Castleton	(518) 732-7205	Binghamton	(607) 722-1582
Fax	(518) 732-4516	Kingsland	(914) 336-4471

Pittsfield (413) 499-5338

HYDRAULIC CONDUCTIVITY TEST DATA

Project Name: LANDFILL SERVICE CORP. POSI-SMELL

Client: Landfill Technologies, Inc.
PO Box 519
West Sand Lake, New York 12196

SMT Project No. 80799

Sample Description: Visual Description:
Gray Cementitious Material
Sample #2
Undisturbed Shelby Tube Specimen:

Date Sampled: 10/23/95
Date Reported: 10/31/95

Date Tested: 10/27/95
Reviewed By: REV RW

Test Standard: ASTM D 5084
Test By: DW

Test Description: Falling Head/Rising
tail Flexible Wall Permeability

RESULTS:

Initial Specimen Properties

Length = 12.36 cm
Diameter = 7.16 cm
Moisture Content = 60.1%
Wet Density = 95.5pcf
Dry Density = 59.7pcf

Test Conditions

Back Pressure = 66.0 psi
Cell Pressure = 70.0 psi
Hydraulic Gradient = 10
Permeant Liquid: Air-less
Tap Water

Remarks:

Hydraulic Conductivity: $k_{20} = 5.8 \times 10^{-6}$ cm/sec

SOIL & MATERIAL TESTING, INC.

Thomas M. Kenney



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CLIENT: Landfill Services Corporation Date Sampled: 12/19/00
CLIENT'S SAMPLE ID: POSI-SHELL Date sample received: 12/27/00
AES sample #: 001227AN01 Samples taken by: G.E./D.B. Location: Chemung County
 MATRIX: Solid Sample grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTE/BK REF</u>	<u>TEST DATE</u>
Flammability Potential	ASTM D 4982-95	Negative		TF-H-22	12/27/00



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CLIENT: Landfill Technologies, Inc. Date Sampled: 07/24/95
CLIENT'S SAMPLE ID: POSI-SHELL (WET) Date sample received: 07/24/95
AES sample #: 950724 001 Samples taken by: Dave Hansen Location: Albany, NY
MATRIX: Product Test grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK REF.</u>	<u>TEST DATE</u>
Paint Filter	SW-846	Negative		MC-X-8	07/24/95

APPROVED BY: Jala Amiri
Report date: 07/26/95



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CHAIN OF CUSTODY RECORD

CLIENT NAME <u>LANDFILL TECHNOLOGIES, INC.</u>	PROJECT NAME (Location)	SAMPLERS: (Name) <u>DAVE HANSEN</u>				
ADDRESS	PO NUMBER	SAMPLERS: (Signature)				
AES SAMPLE NUMBER	CLIENT SAMPLE IDENTIFICATION & LOCATION	DATE SAMPLED	TIME A.m. P.m.	SAMPLE TYPE	NUMBER OF CONT'S	ANALYSIS REQUIRED
960724001	POSI-SHELL (WET)	24 JUL 95 11:46	P	SL	X 1	Free Liquids
			A			Method 909-
			P			
			A			
			P			
			A			
			P			
			A			
			P			
			A			
			P			
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			A			
			P			
			A			
			P			
			A			
			P			
Turnaround Time:	24 hour.	Laboratory Approval:				
Relinquished by: (Signature)	Received by: (Signature)		Date/Time			
<u>Adler</u>						
Relinquished by: (Signature)	Received by: (Signature)		Date/Time			
<u> </u>						
Relinquished by: (Signature)	Received by: (Signature)		Date/Time			
<u> </u>						
Dispatched by: (Signature)	Date/Time	Received for Laboratory by:	Date/Time			
<u> </u>		<u>David Drury</u>	7/24/95 1:20			
Method of Shipment:	Send Report To:		Client Phone No.:			

The Laboratory reserves the right to return hazardous samples to the client or may levy an appropriate fee per container for disposal.

WHITE - Lab Copy

YELLOW - Sampler Copy

PINK - Generator Copy

Adirondack Environmental Services, Inc.

POSI-SHELL® TCLP ANALYSIS

The following table summarizes the TCLP results for the Posi-Shell mixture and its individual components.

Concentration, mg/l

<u>COMPONENT</u>	<u>As</u>	<u>Ba</u>	<u>Cd</u>	<u>Cr</u>	<u>Pb</u>	<u>Hg</u>	<u>Se</u>	<u>Aq</u>
Mineral Binder (CKD)	<0.5	0.38	0.02	<0.05	<0.5	<0.02	<0.1	<0.05
Posi-Pak® Fiber	<0.5	0.43	<0.01	<0.05	<0.5	<0.02	<0.1	<0.05
EarthTone Dye (Brown)	<0.5	0.34	0.02	<0.05	<0.5	<0.02	<0.1	<0.05
Posi-Shell mix (field - fresh)	<0.5	0.22	<0.01	<0.05	<0.5	<0.02	<0.1	<0.05
Posi-Shell mix (fresh - lab)	<0.5	0.30	<0.01	<0.05	<0.5	<0.02	<0.1	<0.05
Posi-Shell mix (one yr. old)	<0.5	0.08	<0.01	0.08	<0.5	<0.02	<0.1	<0.05
Regulatory Level	5.0	100.0	1.0	5.0	5.0	0.2	1.0	5.0



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CLIENT: Landfill Technologies, Inc.

Date Sampled: June 1992

CLIENT'S SAMPLE ID: IND CKD J92

Date sample received: 06/16/92

ARS sample #: 920616 J01

Samples taken by: David Hansen

Location: Albany Landfil

MATRIX: solid waste

grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK</u>	<u>REP</u>	<u>TEST DATE</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4		06/19/9
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/9
Barium-TCLP Extract	EPA-6010	0.38	mg/l	ICP-Y-18		07/01/9
Cadmium-TCLP Extract	EPA-6010	0.02	mg/l	ICP-Y-18		07/01/9
Chromium-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-30B		07/18/9
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/9
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MRT-PAB-39		06/24/9
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18		07/01/9
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18		07/01/9



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CLIENT: Landfill Technologies, Inc.

Date Sampled: June 1992

CLIENT'S SAMPLE ID: Fiber

Date sample received: 06/16/92

APM sample #: 920616 J03

Samples taken by: David Hansen

Location: Albany Landfi

MATRIX: solid waste

grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTE/BK REF</u>	<u>TEST DA</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4	06/19/
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18	07/01/
Barium-TCLP Extract	EPA-6010	0.43	mg/l	ICP-Y-18	07/01/
Cadmium-TCLP Extract	EPA-6010	<0.01	mg/l	ICP-Y-18	07/01/
Chromium-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-30B	07/18/
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18	07/01/
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MET-PAB-39	06/24/
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18	07/01/
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18	07/01/



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CLIENT: Landfill Technologies, Inc. **Date Sampled:** June 1992
CLIENT'S SAMPLE ID: E-Tone **Date sample received:** 06/16/92
AES sample #: 920616 J04 **Samples taken by:** David Hansen **Location:** Albany Landfill
MATRIX: solid waste **grab**

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK</u>	<u>REF</u>	<u>TEST DATE</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4		06/19/92
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Barium-TCLP Extract	EPA-6010	0.34	mg/l	ICP-Y-18		07/01/92
Cadmium-TCLP Extract	EPA-6010	0.02	mg/l	ICP-Y-18		07/01/92
Chromium-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-30B		07/18/92
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MET-PAB-39		06/24/92
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18		07/01/92
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18		07/01/92



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CLIENT: Landfill Technologies, Inc. **Date Sampled:** 06/16/92
CLIENT'S SAMPLE ID: PS-1 WP (POSI-SHELL, FIELD) **Date sample received:** 06/16/92
AES sample #: 920616 J05 **Samples taken by:** David Hansen **Location:** Albany Landfil
MATRIX: solid waste **grab**

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK</u>	<u>REP</u>	<u>TEST DATE</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4		06/19/92
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Barium-TCLP Extract	EPA-6010	0.22	mg/l	ICP-Y-18		07/01/92
Cadmium-TCLP Extract	EPA-6010	<0.01	mg/l	ICP-Y-18		07/01/92
Chromium-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-30R		07/18/92
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MET-PAB-39		06/24/92
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18		07/01/92
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18		07/01/92



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CLIENT: Landfill Technologies, Inc. Date Sampled: 06/16/92
 CLIENT'S SAMPLE ID: PS-1 WL (POSI-SHELL, LAB) Date sample received: 06/16/92
 APS sample #: 920616 J06 Samples taken by: David Hansen Location: Albany Landfill
 MATRIX: solid waste grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK</u>	<u>REP</u>	<u>TEST DATE</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4		06/19/92
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Barium-TCLP Extract	EPA-6010	0.30	mg/l	ICP-Y-18		07/01/92
Cadmium-TCLP Extract	EPA-6010	<0.01	mg/l	ICP-Y-18		07/01/92
Chromium-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-30B		07/18/92
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18		07/01/92
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MET-PAB-39		06/24/92
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18		07/01/92
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18		07/01/92



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CLIENT: Landfill Technologies, Inc. Date Sampled: June 1991
 CLIENT'S SAMPLE ID: PS-JY (POSI-SHELL, 1 YEAR OLD) Date sample received: 06/16/92
 AES sample #: 920616 J07 Samples taken by: David Hansen Location: Albany Landfi
 MATRIX: solid waste grab

<u>PARAMETER PERFORMED</u>	<u>METHOD</u>	<u>RESULT</u>	<u>UNITS</u>	<u>NOTEBOOK REP</u>	<u>TEST DA'</u>
TCLP Extraction	EPA-1311	Complete		EPT-D-4	06/19/
Arsenic-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18	07/01/
Barium-TCLP Extract	EPA-6010	0.08	mg/l	ICP-Y-18	07/01/
Cadmium-TCLP Extract	EPA-6010	<0.01	mg/l	ICP-Y-18	07/01/
Chromium-TCLP Extract	EPA-6010	0.08	mg/l	ICP-Y-30B	07/18/
Lead-TCLP Extract	EPA-6010	<0.5	mg/l	ICP-Y-18	07/01/
Mercury-TCLP Extract	EPA-7470	<0.02	mg/l	MET-PAB-39	06/24/
Selenium-TCLP Extract	EPA-6010	<0.1	mg/l	ICP-Y-18	07/01/
Silver-TCLP Extract	EPA-6010	<0.05	mg/l	ICP-Y-18	07/01/

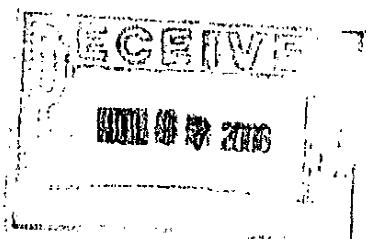
Adirondack Environmental Services, Inc.

Posi-Shell AF, 2 ton mix with portland



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July 13, 2006

Joel E. Lanz
Landfill Service Corporation
2183 Pennsylvania Avenue
Apalachin, NY 13732
TEL: (607) 625-3050
FAX: (607) 625-2689

Work Order No: 060630045

RE: Product testing

Dear Joel E. Lanz:

Adirondack Environmental Services, Inc received 3 samples on 6/30/2006 for the analyses presented in the following report.

There were no problems with the analyses and all associated QC met EPA or laboratory specifications, except if noted.

If you have any questions regarding these tests results, please feel free to call.

Sincerely,

Tara Daniels
Laboratory Manager

ELAP#: 10709
AIHA#: 100307

Qualifiers:
ND - Not Detected at the Reporting Limit
J - Analyte detected below quantitation limits
R - Analyte detected in the associated Method Blank
X - Value exceeds Maximum Contaminant Level

S - Spike Recovery outside accepted recovery limits
R - RPD outside accepted recovery limits
T - Tentatively Identified Compound-Estimated Conc.
E - Value above quantitation range

Adirondack Environmental Services, Inc

Date: 13-Jul-06

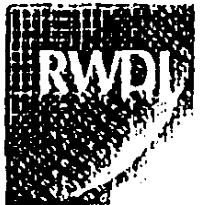
CLIENT: Landfill Service Corporation
Work Order: 060630045
Project: Product testing
PO#:

Client Sample ID: Posi-AF Petri#2
Collection Date:
Lab Sample ID: 060630045-002
Matrix: SOLID

Analyses	Result	PQL	Qual	Units	DF	Date Analyzed	Analyst: SM
TCLP ICP METALS SW6010B/1311							
(Prep: SW1311 - 7/5/2006)							
Aluminum-TCLP	< 1.0	1.0		mg/L	1	7/13/2006 1:18:00 PM	
Antimony-TCLP	< 0.60	0.60		mg/L	1	7/13/2006 1:18:00 PM	
Arsenic-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Barium-TCLP	1.3	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Beryllium-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Boron-TCLP	< 0.50	0.50		mg/L	1	7/13/2006 1:18:00 PM	
Cadmium-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Chromium-TCLP	0.16	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Cobalt-TCLP	< 0.50	0.50		mg/L	1	7/13/2006 1:18:00 PM	
Copper-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Iron-TCLP	< 0.50	0.50		mg/L	1	7/13/2006 1:18:00 PM	
Lead-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Magnesium-TCLP	< 0.50	0.50		mg/L	1	7/13/2006 1:18:00 PM	
Manganese-TCLP	< 0.20	0.20		mg/L	1	7/13/2006 1:18:00 PM	
Molybdenum-TCLP	< 0.10	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Nickel-TCLP	< 0.20	0.20		mg/L	1	7/13/2006 1:18:00 PM	
Selenium-TCLP	< 0.050	0.050		mg/L	1	7/13/2006 1:18:00 PM	
Silver-TCLP	< 0.10	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Thallium-TCLP	< 0.10	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Titanium-TCLP	< 0.10	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Vanadium-TCLP	< 0.20	0.20		mg/L	1	7/13/2006 1:18:00 PM	
Zinc-TCLP	< 0.10	0.10		mg/L	1	7/13/2006 1:18:00 PM	
Zirconium-TCLP	< 0.50	0.50		mg/L	1	7/13/2006 1:18:00 PM	

Qualifiers:
ND - Not Detected at the Reporting Limit
J - Analyte detected below quantitation limits
B - Analyte detected in the associated Method Blank
X - Value exceeds Maximum Contaminant Level

S - Spike Recovery outside accepted recovery limits
R - RPD outside accepted recovery limits
T - Tentatively Identified Compound-Estimated Conc.
E - Value above quantitation range



**ASSESSMENT OF COVER APPLICATION TO
REDUCE AIR EMISSIONS FROM HAZARDOUS
WASTE
LAIDLAW - CORUNNA FACILITY
SARNIA, ONTARIO**

Project Number:

97-411

Date:

December 22, 1997

Submitted By:

Rowan Williams Davies & Irwin Inc.

Project Manager - Brian Handy, B.Sc., C. Chem.

Project Coordinator - Adam Quipp, DET

Principal - David Chadder, Hon. B.Sc., QEP

Submitted to:

Mr. Blake Nesbitt

Laidlaw Environmental Services Limited

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FIGURES

1. INTRODUCTION

Rowan Williams Davies & Irwin Inc. (RWDI) was retained by Laidlaw Environmental Services Limited (Laidlaw) to undertake an assessment of Posi-Shell, a cover material, to reduce air emissions of volatile organic compounds (VOC's), aldehydes, ketones and alcohols from the exposed waste at Laidlaw's Corunna Facility. Posi-Shell is described by its supplier as an aggregate of (recycled) cementitious mineral binder, liquid (water), recycled plastic and cellulose fibres. After curing, the cover is considered to provide an non-permeable cover over the exposed waste, minimising any chemical emissions.

The objectives of this study was to provide an independent assessment of the cover's ability to suppress odourous emissions up to three weeks after application.

The basic tasks undertaken in this study are described below:

- select three sampling locations on the exposed waste at the pit face of the landfill;
- determine the emission rate of target compounds, prior to application, using an isolation flux chamber;
- determine the emission rates of the target compounds one day, two days, one week, two weeks and three weeks after application; and
- assess the emission reduction efficiency of the foam.

2. METHODOLOGY

2.1 Selected Target Compounds

Table 1 presents the list of selected target compounds. The list was based on sampling and headspace analysis conducted by Laidlaw at three Test-Bucket locations on the landfill pit face (Pit Cell #17) during July 11 and 14, 1997 [1]. Figure 1 shows a site map with the three sample locations. Shows a site plan of the facility including the three sample locations. The list represents a cross-section of contaminants that are common to the waste stream at the Corunna facility.

Table 1: List of Target Compounds.

Acetone	o-Xylene
Benzene	p-m-Xylene
Butanediol	Propanal
1-Butanol	Propanol
2-Butanol	Styrene
Butenal	Tetrachlorethylene
Chlorobenzene	1,3,5-Trimethyl Benzene
Cyclohexane	1,2,4-Trimethyl Benzene
Ethyl Benzene	1,2,3-Trimethyl Benzene
Heptane	Toluene
Methyl Ethyl Ketone	Acetaldehyde
2-Methyl Hexane	Difuro-Furan
3-Methyl Hexane	Dichloromethane
Methyl Isobutyl Ketone	Ethanol
Methyl Pentanone	Methyl Butanol

2.2 Sampling Protocol

In the original work plan submitted by RWDI to Laidlaw, it was proposed to conduct continuous VOC measurements over the surface of the pit face, using a PhotoVac Microsid Model MP 1001, in order to select locations with significant emissions which were also safely accessible. These measurements were conducted on July 22, 1997; however, they proved to be inconclusive in locating areas of peak emissions because of relatively low and uniform VOC concentrations above

the pit face. Therefore, it was decided to locate the sampling points in close proximity to the existing Laidlaw Test-Drum locations (see Section 2.1).

The flux chamber was then used to collect samples at these three locations. The flux chamber is shown schematically in Figure 2. It was constructed according to the designer's specifications [2]. The chamber is 71 cm in diameter and 31 cm high and is constructed of 14 gauge stainless steel. All interior and exterior fittings were stainless steel and all lines were made from Teflon tubing. The chamber was equipped with five exit ports (labelled A to E in Figure 2), air and waste temperature probes and a chamber differential pressure gauge. The flux chamber was placed on the surface of the waste and the bottom edge of the chamber was forced a short depth into the waste surface. The interface between the chamber and the surface was covered with common sand to provide the best seal possible. The flux chamber was operated under a slight positive pressure to further prevent outside air entering underneath and into the chamber.

The flux chamber was operated within parameters recommended by the designers [2]. The flux chamber was purged with ultra-high purity nitrogen gas for a minimum of 30 minutes at a rate of 17 l/min ($2.83 \times 10^{-4} \text{ m}^3/\text{s}$). This removed any residual outside air present in the chamber after it was placed on the surface of the waste. The purpose of diluting the chamber air was to establish an equilibrium between gas emissions from the sample surface and the sweep gas entering the chamber. The purge gas was introduced into the flux chamber using Teflon tubing equipped with fifteen, 0.635 mm diameter, downward-facing vent holes. The flow of purge gas (sweep rate) was regulated using a Matheson rotameter, which was calibrated using a Gilibrator automated bubble meter, which is a primary standard airflow calibrator. The total amount of purged gas introduced into the chamber was such that about 99% of the original air was purged from the flux chamber. Once the flux chamber had been purged, samples were drawn from the chamber through the exhaust port using a sample train consisting of a vacuum pump and a calibrated mass flow controller. The samples were collected by on a multi-phase carbon adsorbent TO1 tubes with Tenax provided by Laidlaw Environmental. The on-site Laidlaw laboratory conducted the analysis for the compounds shown in Table 1.

The concentration for each compound, C, was determined using Equation 1:

$$C = M/V \quad (1)$$

where: C = VOC concentration (ng/m^3);

M = mass on tube (ng); and

V = total volume of air sampled (m^3).

The emission flux rate ($\text{ng}/\text{m}^2/\text{s}$) was determined using Equation 2:

$$E = \frac{C \cdot Q}{A} \quad (2)$$

where: E = VOC flux rate ($\text{ng}/\text{m}^2/\text{s}$);

Q = sweep rate of nitrogen into the flux chamber = $2.83 \times 10^{-4} \text{ m}^3/\text{s}$; and

A = surface area enclosed by the flux chamber = 0.40 m^2 .

The flux chamber requires low wind speeds to sample properly. Strong winds may create a region of low pressure on the downwind side of the flux chamber. Winds were light during the flux chamber sampling and no provisions for wind breaks were required.

3. RESULTS

3.1 Sampling Results

The site selection and initial sampling, before cover application, was carried out on July 22, 1997. Covering of the pit face (approximately 90% of the exposed waste) was carried out by the supplier, Landfill Service Corporation, on July 23. After the cover was applied and the curing process was underway, sampling was repeated one day (July 24), two days (July 25), one week (July 31), two weeks (August 7) and three weeks (August 14) after covering. Sections 3.1.1 to 3.1.6 presents pertinent sampling information and the results. Sections 3.2 presents a summary of the results and emission reduction efficiency. All field note information taken during the study have been included in summary tables. All times are given in Eastern Daylight (Savings) Time (EDT).

3.1.1 Site Selection and Pre-Cover Application Sampling

Sample site selection and sampling prior to cover application was conducted on July 22. Table 2 presents a description of the sampling site locations.

Table 2: Sampling Locations.

Sample Number	Location
Site 1	Two metres west of Laidlaw Test-Bucket #3
Site 2	Two metres west of Laidlaw Test-Bucket #2
Site 3	½-metre south of Laidlaw Test-Bucket #1

The sampling parameters (start time, end time, etc.) are presented in Table 3.

Table 3: Sampling Parameters - July 22, 1997.

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	1355	1455	1552
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	1436	1531	1629
Sample End (hours)	1451	1548	1644
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure ("H ₂ O)	0.055	0.050	0.050
Waste Temperature (C)	31	31	36
Ambient Temperature (C)	25	25	27
Wind Speed (m/s)	2.0	2.8	3.0
Weather Conditions	Sunny/Clear D	Sunny/Clear B	Sunny/Clear E
Sample Tube Number			

Table 4 presents the pre-cover sampling results. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location.

Table 4: Pre-Cover Initial Sampling Results - July
22, 1997.

Target Compound	Emission Rate (ng/m ² /s)		
	Site 1	Site 2	Site 3
Acetone	11.8	2.61	14.5
Benzene	0.80	0.58	0.96
1-Butanol	0.64	0.00	1.44
Butanediol	5.58	0.00	18.8
2-Butanol	0.00	0.00	1.91
Butenal	0.48	0.00	0.48
Chlorobenzene	0.16	0.00	0.48
Cyclohexane	0.48	0.00	0.48
Ethyl Benzene	4.62	0.73	3.99
Heptane	0.00	0.00	0.80
Methyl Ethyl Ketone	0.48	1.31	4.15
2-Methyl Hexane	0.00	0.00	0.32
3-Methyl Hexane	0.16	0.00	0.64
Methyl Isobutyl Ketone	2.55	1.31	3.20
Methyl Pentanone	2.55	0.00	0.00
o-Xylene	0.96	0.00	0.00
p,m-Xylene	7.81	1.74	14.8
Propanal	0.00	0.00	7.81
Propanol	0.00	0.00	0.00
Styrene	6.86	1.31	5.74
Tetrachloroethylene	0.48	0.00	10.7
1,3,5-Trimethyl Benzene	0.48	0.00	3.51
1,2,4-Trimethyl Benzene	1.12	0.00	1.43
1,2,3-Trimethyl Benzene	1.12	0.00	2.39
Toluene	13.6	5.51	15.6
Acetaldehyde	0.00	0.00	0.00
Difuro-Furan	0.00	0.00	0.00
Dichloromethane	0.00	0.00	0.00
Ethanol	0.00	0.00	0.00
Methyl Butanol	0.00	0.00	0.00

The table shows that there is some variability between sample sites. This is especially noticeable at sampling Site 2, which generally shows much lower emission rates than the other two sites. Some species predominate in the emissions, for example, acetone, butanediol, ethyl benzene, methyl ethyl ketone, methyl isobutyl ketone, xylene, styrene, tetrachloroethylene and toluene.

3.1.2 One Day After Cover Application - July 24

Cover was applied to the waste material on July 23. Approximately 90% of the pit face was covered. The cover had "cured" to a stable surface by July 24, but it was still wet in spots and the cover appeared to be thin in various locations. It also had a distinct odour. Table 5 presents a description of the cover at the three sampling locations.

Table 5: Description of Sampling Locations on July 24.

Sampling Location	Description
Site 1	<ul style="list-style-type: none"> - Even grey colour - No surface cracks - Approximately 2 cm. thick
Site 2	<ul style="list-style-type: none"> - 10% grey, 90% lime green colour - Approximately 5% of surface cracked - Approximately 1.5 cm. thick
Site 3	<ul style="list-style-type: none"> - 90% grey, 5% green colour - No surface cracks - Approximately 1.5 cm. thick

Table 6 presents the sampling parameters on July 24.

Table 6: Sampling Parameters - July 24

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	0850	1027	1203
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	0924	1057	1235
Sample End (hours)	1024	1200	1335
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure ("H ₂ O)	0.050	0.045	0.040
Waste Temperature (C)	20	23	23
Ambient Temperature (C)	20	21	23
Wind Speed (m/s)	1.8	2.6	1.8
Weather Conditions	Overcast	Overcast	Overcast
Sample Tube Number	F	B	E

Table 7 presents the sampling results for July 24, 1997, one day after cover application. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location.

Table 7: Sampling Results - July 24, 1997.

Target Compound	Emission Rate (ng/m ³ /s)		
	Site 1	Site 2	Site 3
Acetone	1.28	4.32	6.20
Benzene	0.20	0.36	0.00
1-Butanol	0.20	0.24	0.84
Butanediol	1.48	3.56	0.12
2-Butanol	0.14	0.00	0.40
Butenal	0.00	0.00	0.00
Chlorobenzene	0.00	0.08	0.08
Cyclohexane	0.00	0.00	0.00
Ethyl Benzene	0.20	1.56	0.24
Heptane	0.00	0.00	0.00
Methyl Ethyl Ketone	0.64	1.40	1.92
2-Methyl Hexane	0.00	0.00	0.00
3-Methyl Hexane	0.00	0.00	0.00
Methyl Isobutyl Ketone	0.24	1.76	0.36
Methyl Pentanone	0.00	0.00	0.00
o-Xylene	0.00	0.00	0.00
p,m-Xylene	0.16	3.96	0.40
Propanal	0.00	0.00	0.00
Propanol	0.00	0.00	0.40
Styrene	0.20	4.44	0.24
Tetrachlorethylene	0.00	0.24	0.28
1,3,5-Trimethyl Benzene	0.00	0.40	0.16
1,2,4-Trimethyl Benzene	0.00	0.12	0.72
1,2,3-Trimethyl Benzene	0.00	0.24	0.20
Toluene	0.60	8.44	0.84
Acetaldehyde	1.08	0.00	0.00
Difuro-Furan	0.00	1.16	0.00
Dichloromethane	0.00	0.00	0.00
Ethanol	0.00	0.00	0.00
Methyl Butanol	0.00	0.00	8.88

The table shows that, similar to the results on July 22, emissions of some species predominate; however, in general, the emissions rates are greatly reduced. Table 8 shows the percent reduction in the emission rates from July 22 to July 24.

Table 8: Percent Reduction In Emission Rates from July 22 to July 24.

Target Compound	Emission Rate Reduction (%)		
	Site 1	Site 2	Site 3
Acetone	89.2	-65.6	57.3
Benzene	74.9	37.9	100.0
1-Butanol	68.6	NA	41.5
Butanediol	73.5	NA	99.4
2-Butanol	NA	NA	79.1
Butenal	100.0	NA	100.0
Chlorobenzene	100.0	NA	83.3
Cyclohexane	100.0	NA	100.0
Ethyl Benzene	95.7	-115.2	94.0
Heptane	NA	NA	100.0
Methyl Ethyl Ketone	-33.8	-7.3	53.7
2-Methyl Hexane	NA	NA	100.0
3-Methyl Hexane	100.0	NA	100.0
Methyl Isobutyl Ketone	90.6	-34.9	88.7
Methyl Pentanone	100.0	NA	NA
o-Xylene	100.0	NA	NA
p,m-Xylene	98.0	-127.7	97.3
Propanal	NA	NA	100.0
Propanol	NA	NA	NA
Styrene	97.1	-240.3	95.8
Tetrachloroethylene	100.0	NA	88.6
1,3,5-Trimethyl Benzene	100.0	NA	95.4
1,2,4-Trimethyl Benzene	100.0	NA	49.8
1,2,3-Trimethyl Benzene	100.0	NA	91.6
Toluene	95.6	-53.2	94.6
Acetaldehyde	NA	NA	NA
Difuro-Furan	NA	NA	NA
Dichloromethane	NA	NA	NA
Ethanol	NA	NA	NA
Methyl Butanol	NA	NA	NA
Average	87.5	-75.8	86.8

NA: Emission Rate Below Detection Level

The table shows that, on average, the emission rates are reduced by 87.5% at Site 1 and 86.8% at Site 3. However, Site 2 shows some anomalous results, where the emission rates actually increased by 75.8%. The reason for this is unclear, but the surface at Site 2 was found to be different in appearance than at Sites 1 or 3 (i.e., large surface cracks and lime green in colour as opposed to grey at the other locations). It may also be due to the low initial sampling results, which may have been a sampling anomaly.

3.1.3 Two Days After Cover Application - July 25

Table 9 presents the sampling parameters on July 25.

Table 9: Sampling Parameters - July 25.

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	1015	1150	1327
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	1048	1223	1403
Sample End (hours)	1148	1324	1508
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure ("H ₂ O)	0.08	0.06	0.09
Waste Temperature (C)	24	31	36
Ambient Temperature (C)	24	25	28
Wind Speed (m/s)	0.5	1.7	1.6
Weather Conditions	Foggy	Sunny/Hot	Sunny/Hot
Sample Tube Number	E	D	F

The cover appeared to be slightly harder and exhibited less odour. Table 10 presents the sampling results for July 25, 1997, two days after cover application. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location. The internal chamber pressures were found to be higher than recommended by the designer. Correction factors, supplied by the designers, were applied to the emission rates to account for this slight overpressure condition.

Table 10: Sampling Results - July 25, 1997.

Target Compound	Emission Rate (ng/m ³ /s)		
	Site 1	Site 2	Site 3
Acetone	7.91	4.41	10.03
Benzene	0.70	0.32	0.55
1-Butanol	0.61	0.00	0.99
Butanediol	0.00	1.81	26.12
2-Butanol	0.00	0.00	0.22
Butenal	0.17	0.24	0.00
Chlorobenzene	0.17	0.08	0.33
Cyclohexane	0.00	0.00	0.00
Ethyl Benzene	0.35	1.38	0.55
Heptane	0.00	0.24	0.00
Methyl Ethyl Ketone	0.17	0.20	0.11
2-Methyl Hexane	0.00	0.12	0.00
3-Methyl Hexane	0.00	0.00	0.00
Methyl Isobutyl Ketone	0.87	1.50	1.21
Methyl Pentanone	0.26	1.14	4.96
o-Xylene	0.00	0.00	0.55
p,m-Xylene	0.44	3.11	1.43
Propanal	0.00	0.00	0.00
Propanol	0.00	0.00	5.29
Styrene	0.44	4.68	0.00
Tetrachlorethylene	0.00	0.51	1.43
1,3,5-Trimethyl Benzene	0.00	0.32	0.00
1,2,4-Trimethyl Benzene	0.00	0.21	0.00
1,2,3-Trimethyl Benzene	0.00	0.39	0.00
Toluene	1.30	7.79	2.75
Acetaldehyde	5.13	0.00	6.50
Difuro-Furan	0.00	0.00	0.00
Dichloromethane	0.00	0.63	0.00
Ethanol	0.00	0.00	7.72
Methyl Butanol	0.00	0.00	0.00

Similar to the previous days sampling results, the emission rates are still greatly reduced compared to the pre-covering results on July 22. Table 11 shows the percent reduction in the emission rates from July 22 to July 25.

Table 11: Percent Reduction In Emission Rates from July 22 to July 25.

Target Compound	Emission Rate Reduction (%)		
	Site 1	Site 2	Site 3
Acetone	32.9	-68.9	76.8
Benzene	12.7	45.7	80.7
1-Butanol	4.6	NA	76.8
Butanediol	99.9	NA	53.5
2-Butanol	NA	NA	96.1
Butenal	63.6	NA	99.9
Chlorobenzene	NA	NA	76.8
Cyclohexane	99.9	NA	99.9
Ethyl Benzene	92.5	-90.0	95.4
Heptane	NA	NA	99.9
Methyl Ethyl Ketone	63.6	84.9	99.1
2-Methyl Hexane	NA	NA	99.9
3-Methyl Hexane	99.9	NA	99.9
Methyl Isobutyl Ketone	65.9	-11.6	87.3
Methyl Pentanone	89.8	NA	NA
o-Xylene	99.9	NA	NA
p-,m-Xylene	94.4	-78.7	96.8
Propanal	NA	NA	99.9
Propanol	NA	NA	NA
Styrene	93.7	-258.9	99.9
Tetrachlorethylene	99.9	NA	95.5
1,3,5-Trimethyl Benzene	99.9	NA	99.9
1,2,4-Trimethyl Benzene	99.9	NA	99.9
1,2,3-Trimethyl Benzene	99.9	NA	99.9
Toluene	95.6	-41.4	94.1
Acetaldehyde	NA	NA	NA
Difuro-Furan	NA	NA	NA
Dichloromethane	NA	NA	NA
Ethanol	NA	NA	NA
Methyl Butanol	NA	NA	NA
Average	75.3	-52.7	82.3
NA: Emission Rate Below Detection Level			

The table shows that at Sites 1 and 2, the average reduction in the emission rates has decreased slightly (i.e., 87.5% to 75.3% at Site 1 and 86.8% to 82.3% at Site 2. This slight decrease may be due to the fact that any suppression of emissions due to moisture is absent as the waste and cover dries out and the fact that the cover has not yet completely cured, statistical variations in the analysis, or because of additional curing of the cover producing a more impervious surface. Site 2 still shows anomalous results with an increase in the average emission rate; however, the increase was slightly smaller (i.e., 52.7%, down from 75.8%) than was found after first day

(post-cover).

3.1.4 One Week After Cover Application - July 31

Table 12 presents the sampling parameters on July 31.

Table 12: Sampling Parameters - July 31.

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	1020	1155	1328
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	1040	1225	1353
Sample End (hours)	1140	1325	1453
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure ("H ₂ O)	0.04	0.06	0.06
Waste Temperature (C)	31	40	42
Ambient Temperature (C)	23	26	28
Wind Speed (m/s)	1.0	1.7	2.0
Weather Conditions	Sunny C	Sunny/Hot D	Sunny/Hot E
Sample Tube Number			

The cover surface was noticeably harder, with very little odour. Also no additional cracking of the surface was evident. Table 13 presents the sampling results for July 31, 1997, one week after cover application. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location.

Table 13: Sampling Results - July 31, 1997.

Target Compound	Emission Rate (ng/m ³ /s)		
	Site 1	Site 2	Site 3
Acetone	4.92	5.08	10.92
Benzene	0.40	0.08	2.76
1-Butanol	0.28	0.00	1.96
Butanediol	0.00	0.00	0.00
2-Butanol	0.40	0.00	0.24
Butenal	0.00	0.00	0.52
Chlorobenzene	0.00	0.00	0.00
Cyclohexane	0.00	0.00	0.00
Ethyl Benzene	1.56	0.00	0.12
Heptane	0.00	0.00	0.00
Methyl Ethyl Ketone	2.44	0.00	0.12
2-Methyl Hexane	0.00	0.00	0.00
3-Methyl Hexane	0.00	0.00	0.00
Methyl Isobutyl Ketone	1.20	0.00	0.44
Methyl Pentanone	0.00	0.00	0.00
o-Xylene	0.00	0.00	0.12
p,m-Xylene	1.56	0.00	0.36
Propanal	0.00	0.00	0.00
Propanol	0.00	0.00	0.00
Styrene	1.56	0.00	0.00
Tetrachlorethylene	0.28	0.08	0.40
1,3,5-Trimethyl Benzene	0.00	0.00	0.00
1,2,4-Trimethyl Benzene	0.00	0.00	0.00
1,2,3-Trimethyl Benzene	0.00	0.00	0.00
Toluene	4.04	0.08	0.84
Acetaldehyde	0.00	0.00	0.00
Difuro-Furan	0.00	0.00	0.00
Dichloromethane	0.76	2.52	0.00
Ethanol	0.00	0.00	0.00
Methyl Butanol	7.60	0.00	0.16

The results show that, although the cover surface had appeared to have undergone additional curing, the emission rates have increased for the majority of compounds compared to the measurements conducted a week ago on July 25. However, emissions from Site 2 have significantly decreased. This is also evident in Table 14, which shows the percent reduction in the emission rates from July 22 to July 31.

Table 14: Percent Reduction In Emission Rates from July 22 to July 31.

Target Compound	Emission Rate Reduction (%)		
	Site 1	Site 2	Site 3
Acetone	58.3	-94.7	24.7
Benzene	49.8	86.2	-188.5
1-Butanol	56.1	NA	-36.6
Butanediol	73.5	NA	99.9
2-Butanol	NA	NA	87.5
Butenal	99.9	NA	-8.7
Chlorobenzene	99.9	NA	99.9
Cyclohexane	99.9	NA	99.9
Ethyl Benzene	66.3	99.9	97.0
Heptane	NA	NA	99.9
Methyl Ethyl Ketone	-410.1	99.9	97.1
2-Methyl Hexane	NA	NA	99.9
3-Methyl Hexane	99.9	NA	99.9
Methyl Isobutyl Ketone	53.0	99.9	86.2
Methyl Pentanone	99.9	NA	NA
o-Xylene	99.9	NA	NA
p-,m-Xylene	80.0	99.9	97.6
Propanal	NA	NA	99.9
Propanol	NA	NA	NA
Styrene	77.2	99.9	99.9
Tetrachlorethylene	41.5	NA	96.3
1,3,5-Trimethyl Benzene	99.9	NA	99.9
1,2,4-Trimethyl Benzene	99.9	NA	99.9
1,2,3-Trimethyl Benzene	99.9	NA	99.9
Toluene	70.2	98.5	94.6
Acetaldehyde	NA	NA	NA
Difuro-Furan	NA	NA	NA
Dichloromethane	NA	NA	NA
Ethanol	NA	NA	NA
Methyl Butanol	NA	NA	NA
Average	55.7	73.7	70.3
NA: Emission Rate Below Detection Level			

The table shows that the average reduction in the emission rate has changed from 75.3% on July 25 to 55.7% on July 31 at Site 1. Similarly, at Site 3, the average emission rate has changed from 82.3% on July 25 to 70.3% on July 31. However, the emission rate at Site 2 is now comparable to the other sites with an emission rate reduction, compared to the initial measurements on July 22 of 73.7%. The reason for the slight increase in the emissions at Sites 2 and 3 is unclear. There was no indication from observation of the cover surface that deterioration had taken place. In fact, the surface was found to be harder and looked more likely to be less permeable. Therefore, the

difference may be due to just statistical variation in the analysis from sample to sample. There is also no explanation in the results from Site 2, as again there was no evidence of change in the cover surface at this location.

3.1.5 Two Weeks After Cover Application - August 7

Table 15 presents the sampling parameters on August 7.

Table 15: Sampling Parameters - August 7.

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	0910	1122	1303
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	1020	1153	1344
Sample End (hours)	1120	1301	1444
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure (^H ₂ O)	0.02	0.04	0.03
Waste Temperature (C)	22	30	30
Ambient Temperature (C)	24	26	26
Wind Speed (m/s)	1.5	2.5	2.0
Weather Conditions	Sunny	Sunny/Hot	Sunny/Hot
Sample Tube Number	B	D	F

There was little change in the cover surface from that observed on July 31. A few cracks had appeared, but they were relatively small. Table 16 presents the sampling results for August 7, two weeks after cover application. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location.

Table 16: Sampling Results - August 7.

Target Compound	Emission Rate (ng/m ³ /s)		
	Site 1	Site 2	Site 3
Acetone	1.84	6.60	6.04
Benzene	0.12	0.00	0.20
1-Butanol	0.12	0.00	0.20
Butanediol	0.00	0.00	0.00
2-Butanol	0.00	0.36	0.56
Butenal	0.00	0.00	0.00
Chlorobenzene	0.00	0.00	0.00
Cyclohexane	0.00	0.00	0.00
Ethyl Benzene	0.52	2.36	0.20
Heptane	0.00	0.32	0.00
Methyl Ethyl Ketone	0.76	0.00	2.32
2-Methyl Hexane	0.00	0.00	0.00
3-Methyl Hexane	0.00	0.00	0.00
Methyl Isobutyl Ketone	0.44	2.20	0.44
Methyl Pentanone	0.00	0.00	0.00
o-Xylene	0.00	0.00	0.20
p,m-Xylene	0.60	5.32	0.68
Propanal	0.00	0.00	0.00
Propanol	0.00	0.00	0.00
Styrene	0.36	4.84	0.00
Tetrachlorethylene	0.16	0.68	0.64
1,3,5-Trimethyl Benzene	0.00	0.56	0.00
1,2,4-Trimethyl Benzene	0.00	0.48	0.00
1,2,3-Trimethyl Benzene	0.00	0.00	0.00
Toluene	2.40	10.12	1.68
Acetaldehyde	0.00	0.00	0.00
Difuro-Furan	0.00	0.00	0.00
Dichloromethane	0.32	1.36	0.00
Ethanol	0.00	0.00	0.00
Methyl Butanal	1.04	5.40	1.64

The emission rates in Table 16 are similar to the emission rates measured on July 24 and 25. Therefore it appears that the results on July 31 may have been an anomaly. This is evident in Table 17, which shows the percent reduction in the emission rates from July 22 to August 7.

Table 17: Percent Reduction In Emission Rates from July 22 to August 7.

Target Compound	Emission Rate Reduction (%)		
	Site 1	Site 2	Site 3
Acetone	34.9	-100.0	33.4
Benzene	84.9	99.9	79.1
1-Butanol	81.2	NA	86.1
Butanediol	99.9	NA	99.9
2-Butanol	NA	NA	70.7
Butenal	99.9	NA	99.9
Chlorobenzene	99.9	NA	99.9
Cyclohexane	99.9	NA	99.9
Ethyl Benzene	88.8	-225.6	95.0
Heptane	NA	NA	99.9
Methyl Ethyl Ketone	-58.9	99.9	44.0
2-Methyl Hexane	NA	NA	99.9
3-Methyl Hexane	99.9	NA	99.9
Methyl Isobutyl Ketone	82.8	-68.6	86.2
Methyl Pentanone	99.9	NA	NA
o-Xylene	99.9	NA	NA
p,m-Xylene	92.3	-205.9	95.4
Propanal	NA	NA	99.9
Propanol	NA	NA	NA
Styrene	94.7	-271.0	99.9
Tetrachlorethylene	66.6	NA	94.0
1,3,5-Trimethyl Benzene	99.9	NA	99.9
1,2,4-Trimethyl Benzene	99.9	NA	99.9
1,2,3-Trimethyl Benzene	99.9	NA	99.9
Toluene	82.3	-83.7	89.2
Acetaldehyde	NA	NA	NA
Difuro-Furan	NA	NA	NA
Dichloromethane	NA	NA	NA
Ethanol	NA	NA	NA
Methyl Butanol	NA	NA	NA
Average	84.9	-101.0	90.8
NA: Emission Rate Below Detection Level			

The table shows that the average reduction in the emission rate is similar to the reductions measured on July 24 and 25. The average emission rate reduction at Site 1 was 84.9%, compared to 87.5% on July 24, 88.3% on July 25 and 55.7% on August 7. At Site 3, the average emission rate reduction was 90.8%, compared to 86.8% on July 24, 92.2% on July 25 and 70.3% on July 31. However, the average emission rate at Site 2 is again showing an increase compared to the original measurements on July 22. Therefore, it appears that the measurements conducted on July 31 were anomalous.

3.1.6 Three Weeks After Cover Application - August 14

Table 18 presents the sampling parameters on August 14.

Table 18: Sampling Parameters - August 14.

Parameter	Site 1	Site 2	Site 3
Purge Start (hours)	1030	1225	1400
Sweep Rate (l/min)	17.2	17.2	17.2
Sample Start (hours)	1122	1256	1344
Sample End (hours)	1222	1356	1444
Sample Flow Rate (ml/min)	300	300	300
Internal Pressure ("H ₂ O)	0.025	0.05	0.045
Waste Temperature (C)	24	29	30
Ambient Temperature (C)	25	25	26
Wind Speed (m/s)	2.5	2.7	2.5
Weather Conditions	Sunny D	Sunny/Hot E	Sunny/Hot F
Sample Tube Number			

Similar to the observations made on August 7, there was little change in the cover surface. Table 19 presents the sampling results for August 14, three weeks after cover application. The table shows the emission rate in ng/m³/s for the target compounds at each sampling location.

Table 19: Sampling Results - August 14.

Target Compound	Emission Rate (ng/m ² /s)		
	Site 1	Site 2	Site 3
Acetone	0.36	3.12	4.76
Benzene	0.08	0.36	0.16
1-Butanol	0.00	0.00	0.28
Butanediol	0.00	0.00	0.00
2-Butanol	0.20	0.00	1.24
Butenal	0.00	0.68	0.20
Chlorobenzene	0.00	0.00	0.00
Cyclohexane	0.00	0.00	0.00
Ethyl Benzene	0.04	1.84	0.08
Heptane	0.00	0.00	0.00
Methyl Ethyl Ketone	0.20	0.96	2.16
2-Methyl Hexane	0.00	0.00	0.00
3-Methyl Hexane	0.00	0.00	0.00
Methyl Isobutyl Ketone	0.16	1.08	0.32
Methyl Pentanone	0.00	0.00	0.00
o-Xylene	0.00	0.00	0.00
p,m-Xylene	0.08	3.16	0.16
Propanal	0.00	0.00	0.00
Propanol	0.00	0.00	0.00
Styrene	0.00	2.88	0.08
Tetrachlorethylene	0.00	0.28	0.00
1,3,5-Trimethyl Benzene	0.00	0.00	0.00
1,2,4-Trimethyl Benzene	0.00	0.00	0.00
1,2,3-Trimethyl Benzene	0.00	0.00	0.00
Toluene	0.20	7.20	0.48
Acetaldehyde	0.00	0.00	0.00
Difuro-Furan	0.00	0.00	0.00
Dichloromethane	0.00	1.12	0.00
Ethanol	0.00	0.00	0.00
Methyl Butanol	0.36	4.84	12.96

The emission rates in Table 19 are similar to the emission rates measured the previous week on August 7. In fact, with the exception of methyl butanol at Site 3, the emission rates are all slightly lower. This is also shown in Table 20, which presents the percent reduction in the emission rates from July 22 to August 17.

Table 20: Percent Reduction In Emission Rates from July 22 to August 14.

Target Compound	Emission Rate Reduction (%)		
	Site 1	Site 2	Site 3
Acetone	96.9	-19.6	67.2
Benzene	90.0	37.9	83.3
1-Butanol	99.9	NA	80.5
Butanediol	99.9	NA	99.9
2-Butanol	NA	NA	35.2
Butenal	99.9	NA	58.2
Chlorobenzene	99.9	NA	99.9
Cyclohexane	99.9	NA	99.9
Ethyl Benzene	99.1	-153.9	98.0
Heptane	NA	NA	99.9
Methyl Ethyl Ketone	58.2	26.4	47.9
2-Methyl Hexane	NA	NA	99.9
3-Methyl Hexane	99.9	NA	99.9
Methyl Isobutyl Ketone	93.7	17.2	90.0
Methyl Pentanone	99.9	NA	NA
o-Xylene	99.9	NA	NA
p-,m-Xylene	99.0	-81.7	98.9
Propanal	NA	NA	99.9
Propanol	NA	NA	NA
Styrene	99.9	-120.8	98.6
Tetrachlorethylene	99.9	NA	99.9
1,3,5-Trimethyl Benzene	99.9	NA	99.9
1,2,4-Trimethyl Benzene	99.9	NA	99.9
1,2,3-Trimethyl Benzene	99.9	NA	96.9
Toluene	98.5	-30.7	NA
Acetaldehyde	NA	NA	NA
Difuro-Furan	NA	NA	NA
Dichloromethane	NA	NA	NA
Ethanol	NA	NA	NA
Methyl Butanol	NA	NA	NA
Average	96.7	-40.6	88.8

NA: Emission Rate Below Detection Level

The table shows similar results to the previous weeks measurements at Sites 1 and 3. There was a slight improvement at Site 1 where the average reduction increased from 84.9% to 96.7%. At Site 2 the average reduction dropped from 90.8 % to 88.8%, primarily due to the increased emissions of methyl butanol. Site 2 showed the similar emissions increase compared to the initial measurements on July 22.

3.2 Summary of Results

Table 21 presents a summary of the percent reduction in emissions for selected compounds during all five sampling periods. Compounds that were not detected during any of the sampling periods (e.g., dichloromethane, ethanol, etc.) were omitted from the table. Summary results for Site 2 have not been presented due to the anomalous nature of the data. It is suspected that the anomalous results from Site 2 were due to either poor application of cover at this location (see Table 5, Section 3.1.2) or a chemical reaction between the cover and the waste.

the emissions had generally increased, but a steady reduction was found in emissions over the next 3 weeks at Site 1. The findings were similar at Site 3 however, there was slightly more variability for some of the select compounds. The figures clearly show an overall reduction in emission rates over the study period particularly after the cover material had the opportunity to cure. Therefore, it appears that, during the 21-day period of this study, the Posi-Shell cover material appeared to be an effective barrier, reducing airborne emissions from the stored waste.

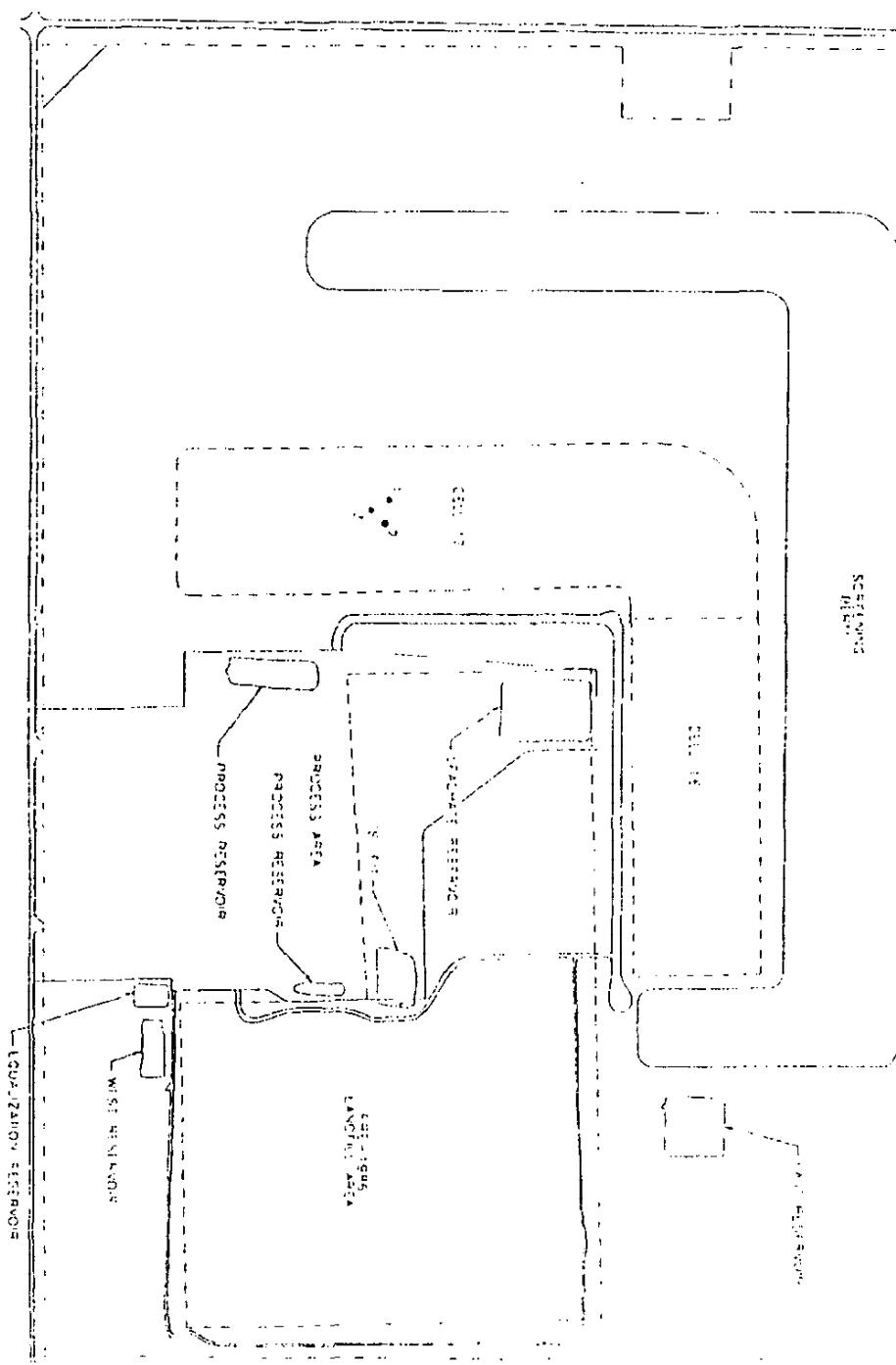
4. CONCLUSIONS

RWDI performed an assessment of a cover application material called Posi-Shell to reduce air emissions of volatile organic compounds, aldehydes, ketones and alcohols from the exposed waste at Laidlaw's Corunna Facility. The study involved sampling the emissions of target compounds from the pit face using an isolation flux chamber. Three sample positions were studied.

The results indicated that, over the 21-day study period, emissions of the target compounds from the two sites at the pit face were reduced by about 89 to 97%. Anomalous findings were encountered at the second location which appeared to be related to a chemical reaction with the waste that may have changed the binding characteristics of the Posi-Shell. With minor exceptions, the cover appeared to form a resilient surface, free from major cracks, after curing. When properly applied, the cover application was demonstrated to be an effective cover material, capable of dramatically reducing emissions for the target compounds.

5. REFERENCES

1. Fax transmittal from Mr. Blake Nesbitt, Laidlaw Environmental Services, to Mr. David Chadder, RWDI on July 15, 1997.
2. Reinhart, D. R., D. C. Cooper and B. L. Walker. 1992. "Flux Chamber Design and Operation for the Measurement of Solid Waste Landfill Gas Emission Rates". Journal of Air and Waste Management Association. 42:1067-70.

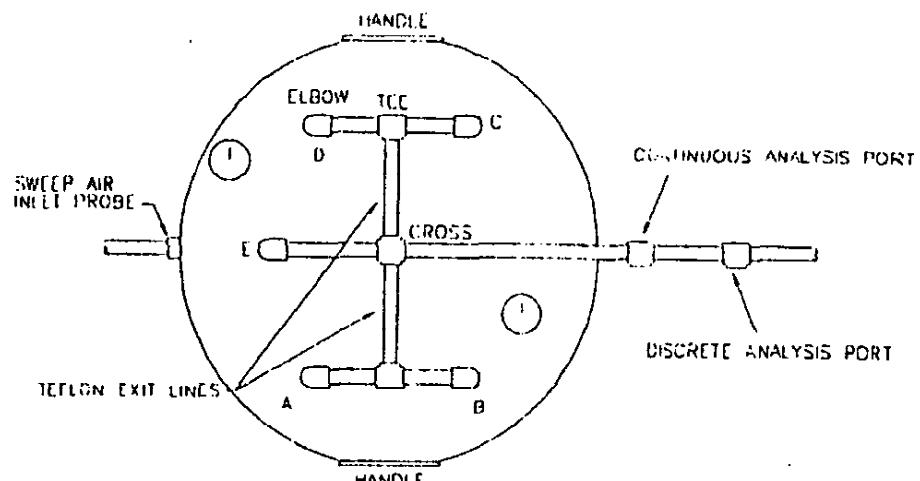


Flux Chamber Sample Locations

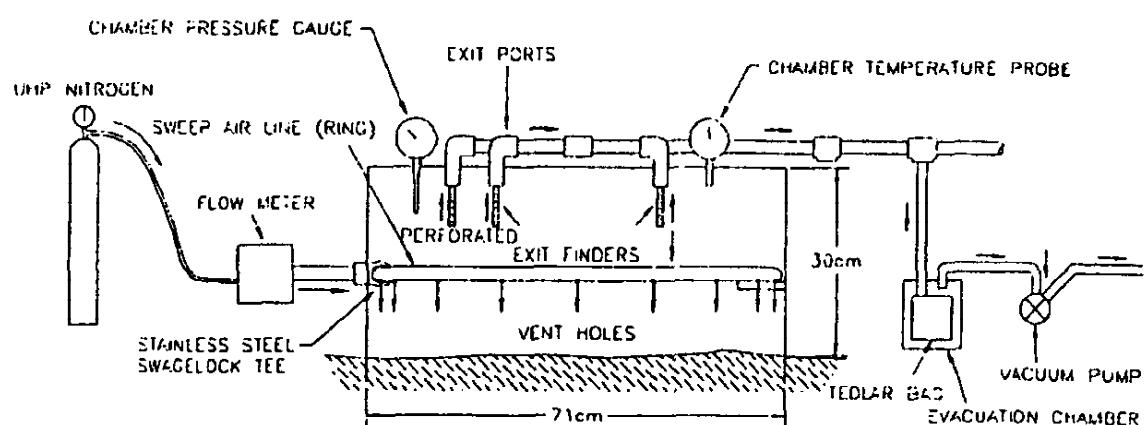
	Drawn by SML figure 1
Scale	Approx. 1:7,000
Date	Oct. 30, 1997
Job No	97-411

RWDI

Laidlaw Cover Application - Corunna, Ontario



Top View



Side View

Schematic Drawing
Flux Chamber Sampling Assembly

Laidlaw Cover Application - Corunna, Ontario

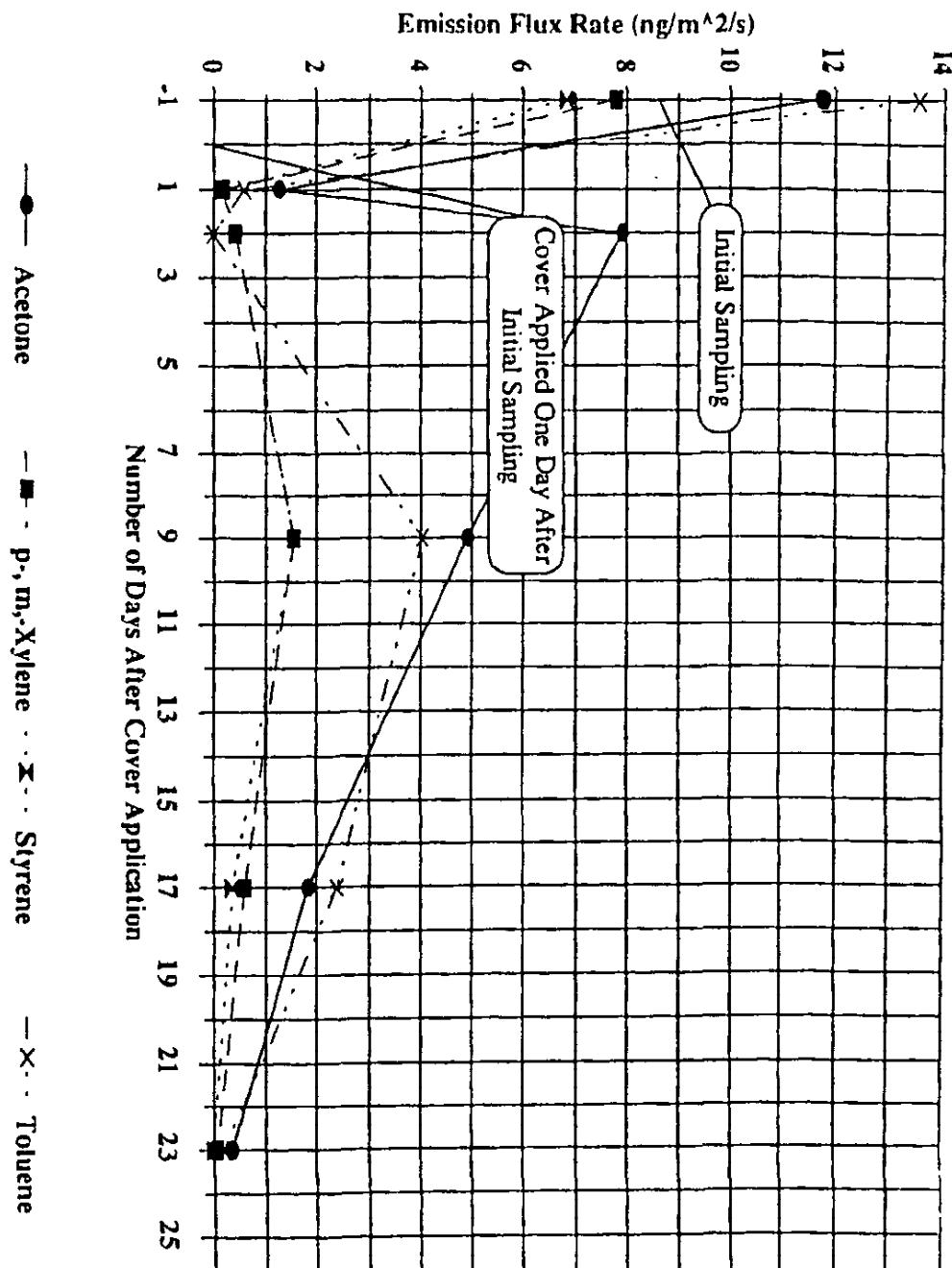
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Scale: N.T.S.

Job No. 97-411

Date: Oct. 29, 1997

RWDI



Emission Flux Rates for Select Compounds - Site 1

Figure:

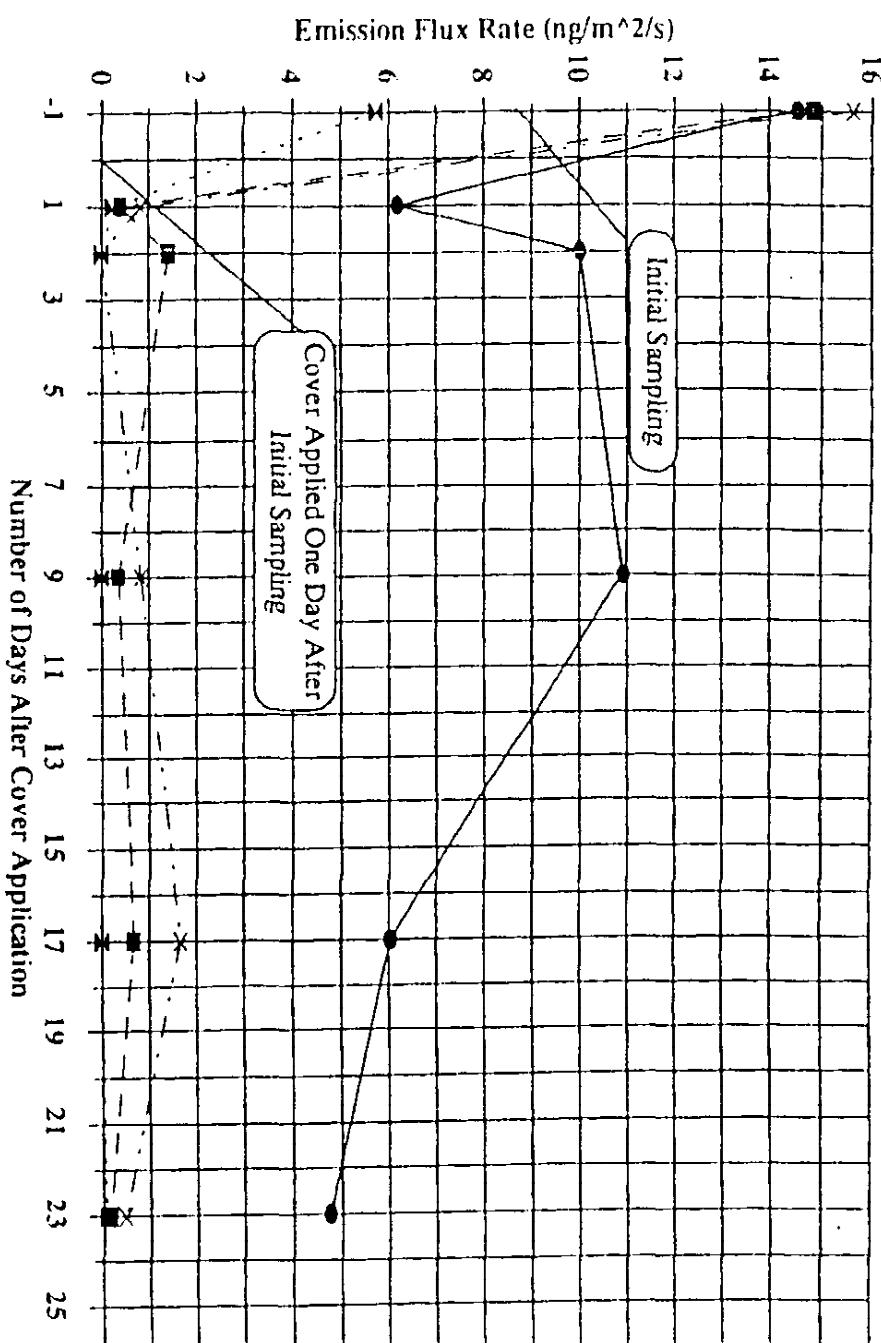
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RWDI

Laidlaw Cover Application - Conuma, Ontario

Job No. 97-411

Date: Oct. 30, 1997



Emission Flux Rates for Select Compounds - Site 3

Figure:

4

Ladlaw Cover Application - Cornwall, Ontario

Job No. 97-411

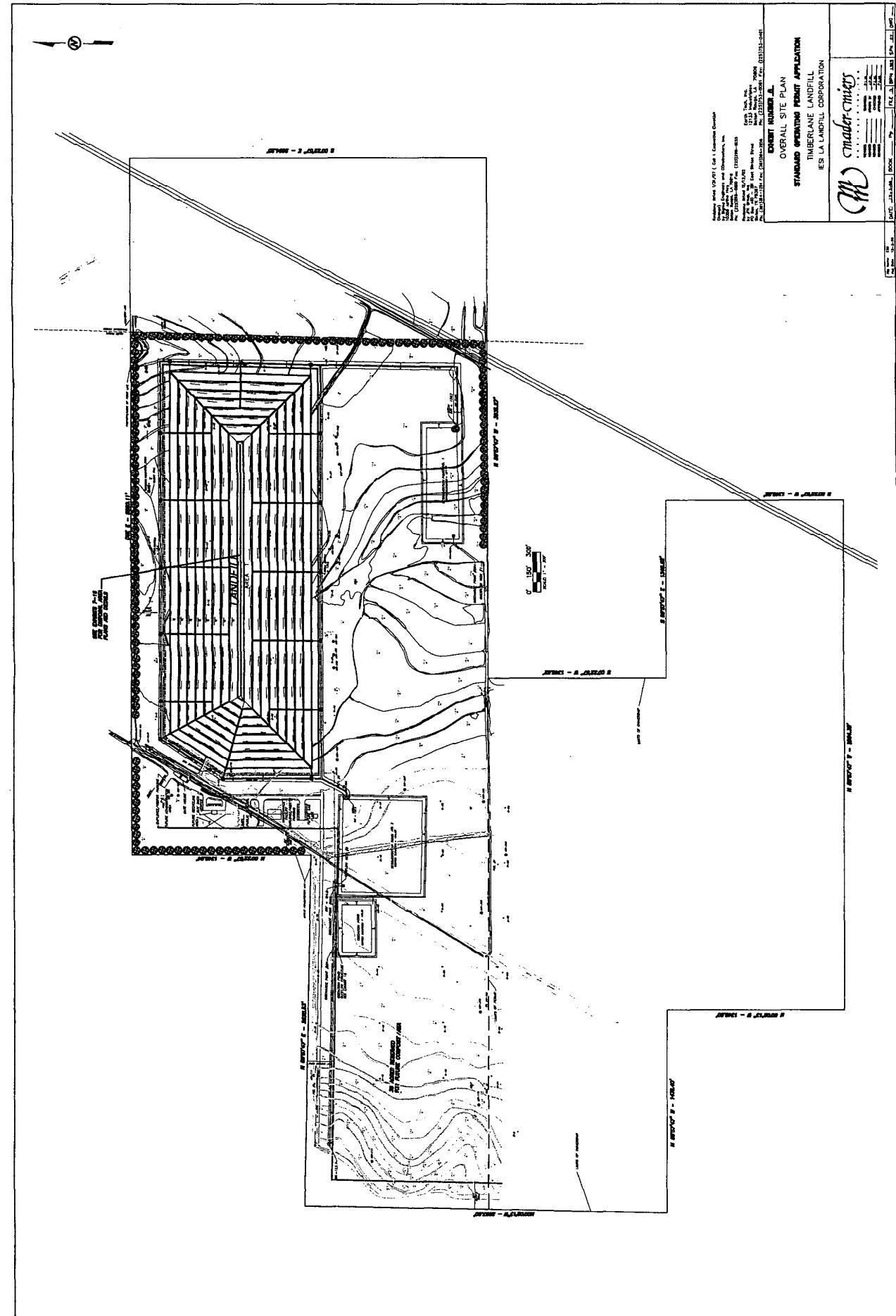
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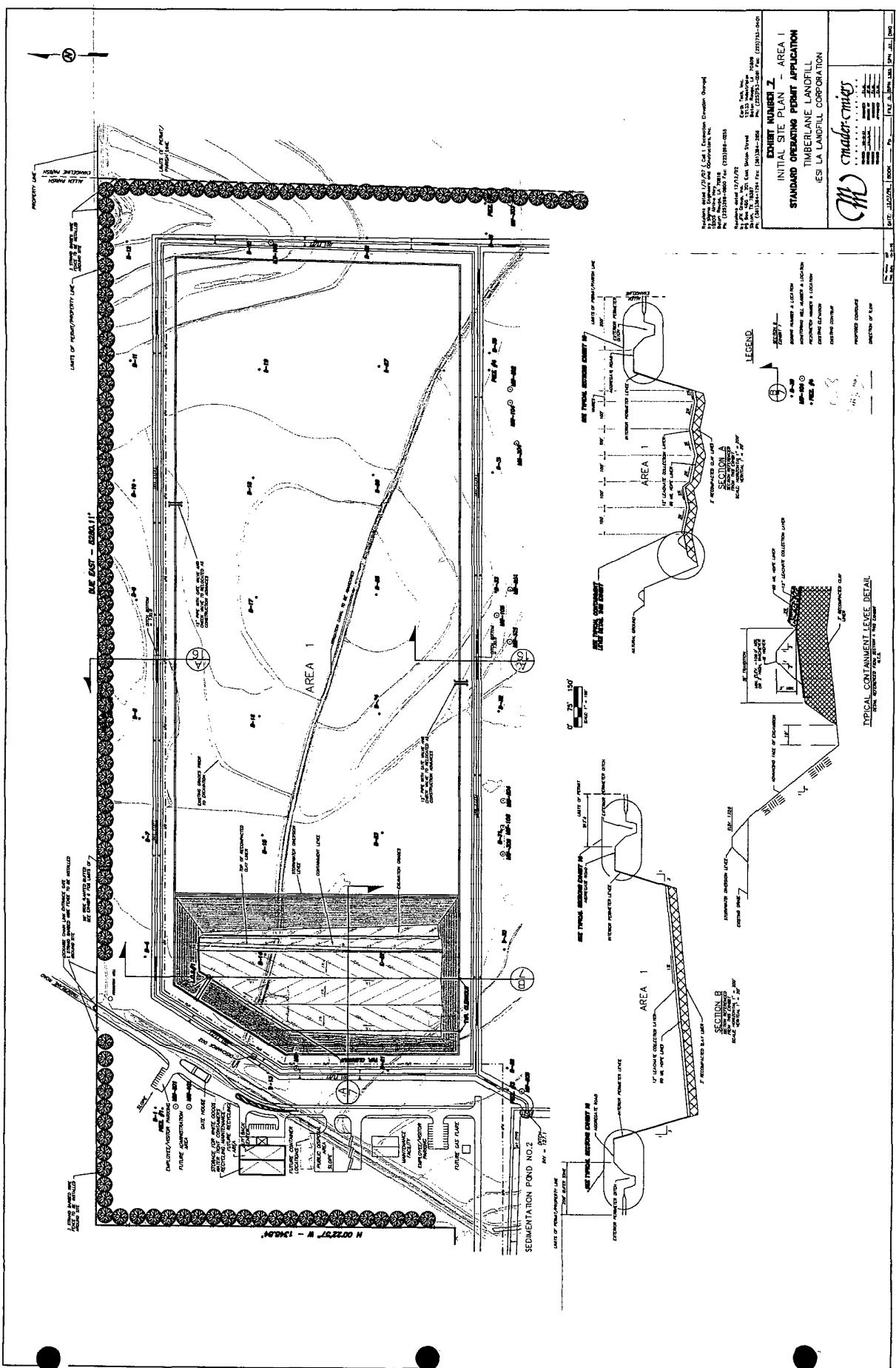
RWDI

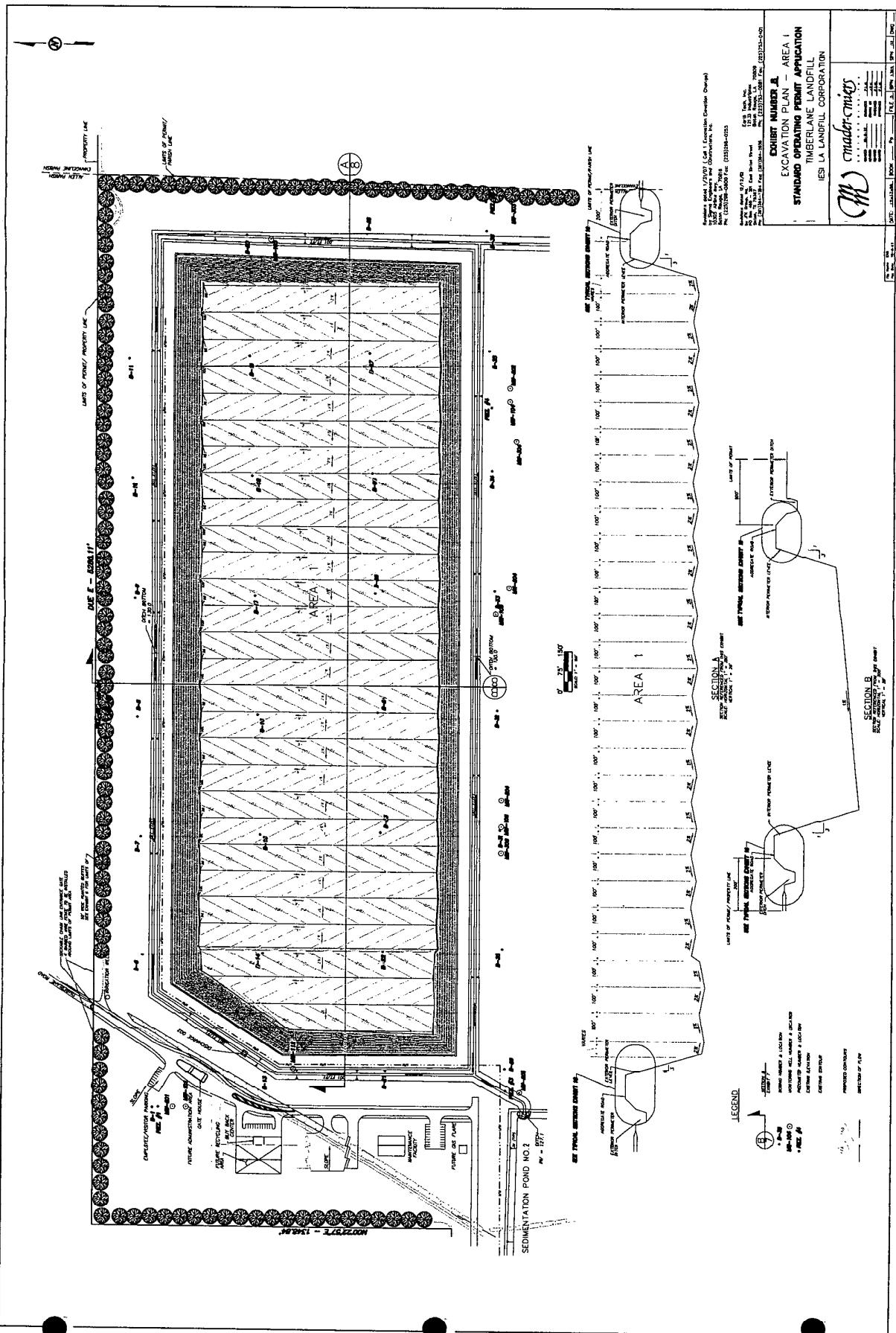
EXHIBITS

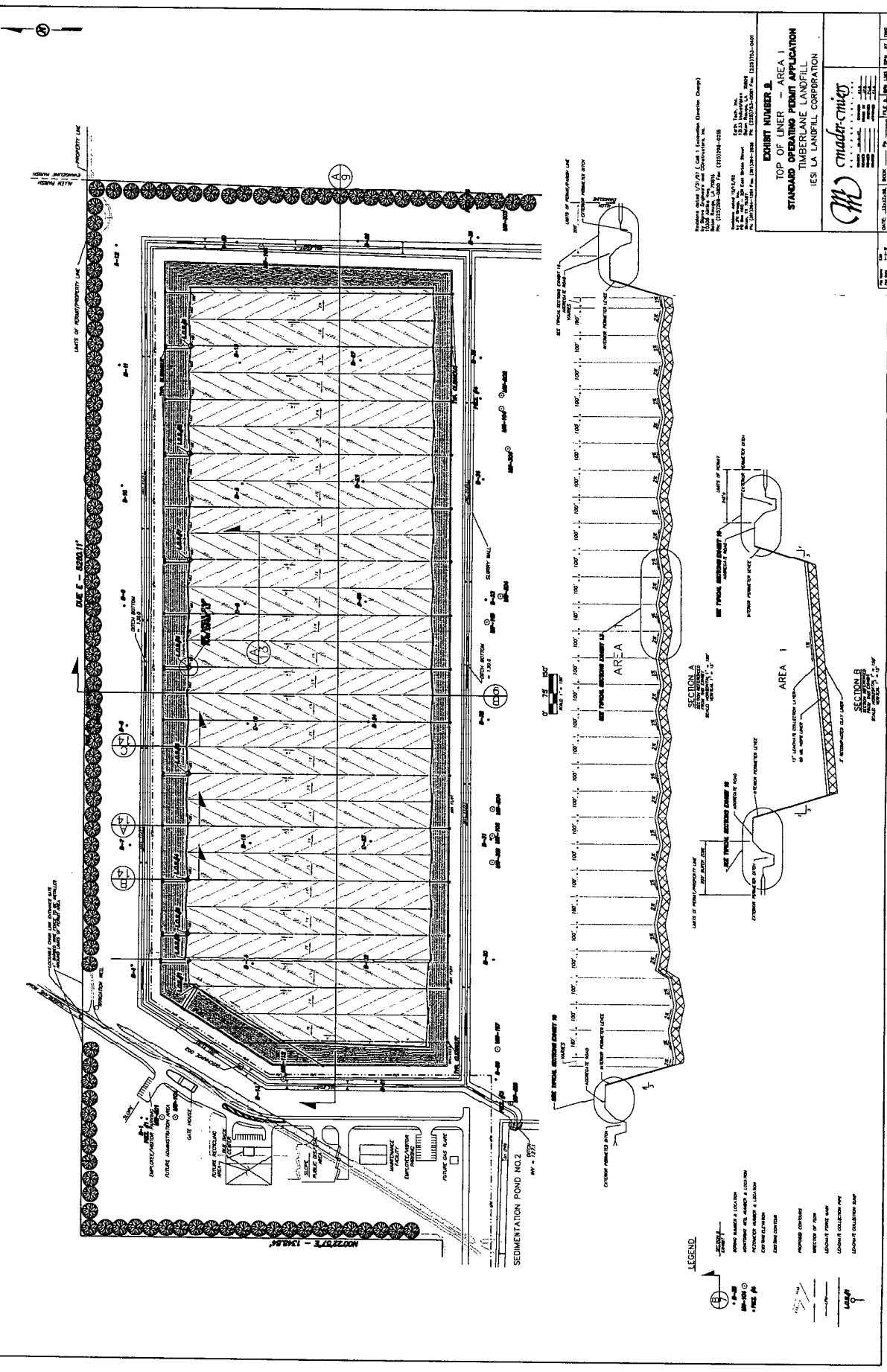
IESI TIMBERLANE LANDFILL

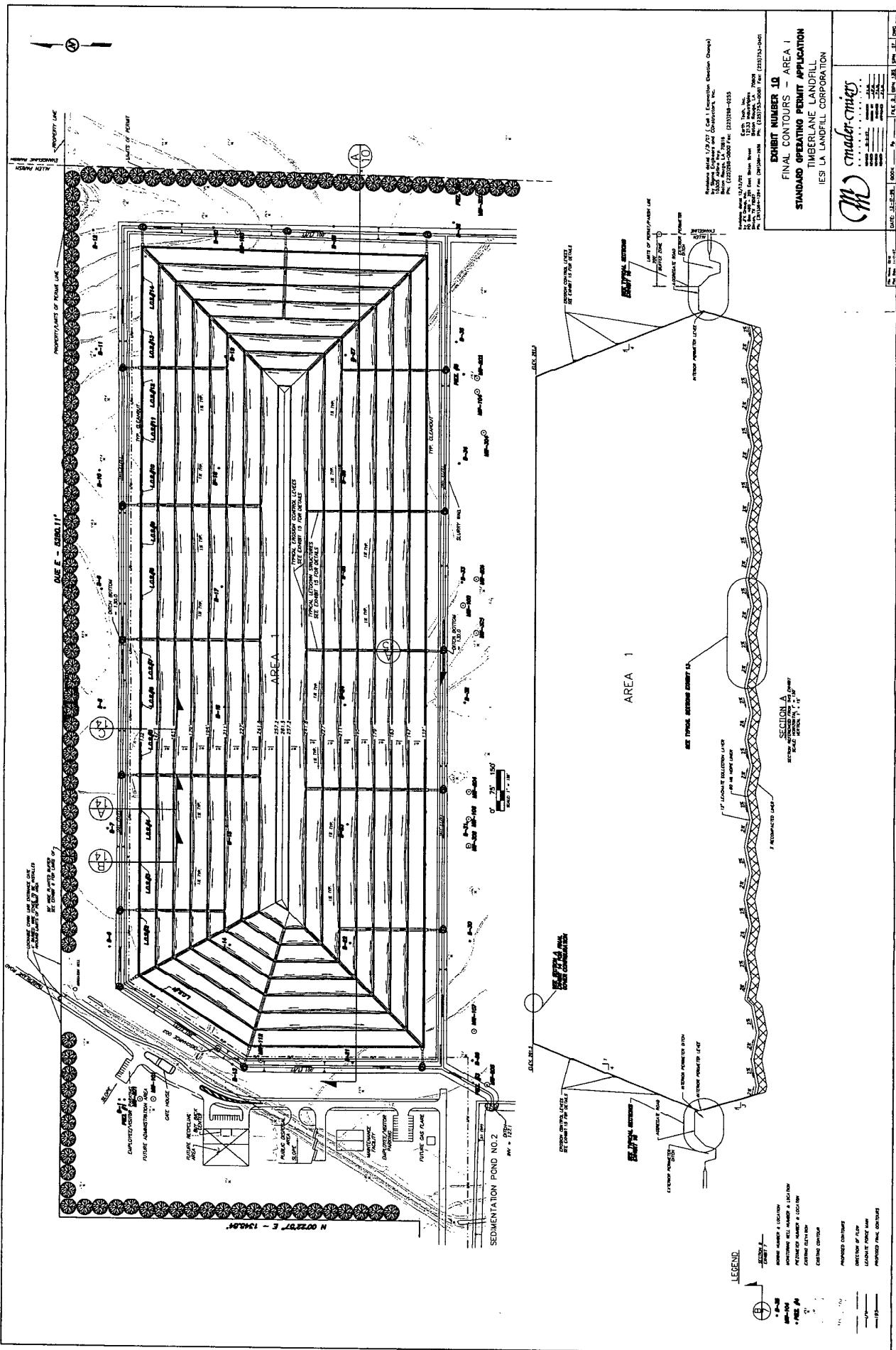
SIGMA ENGINEERS & CONSTRUCTORS, INC.

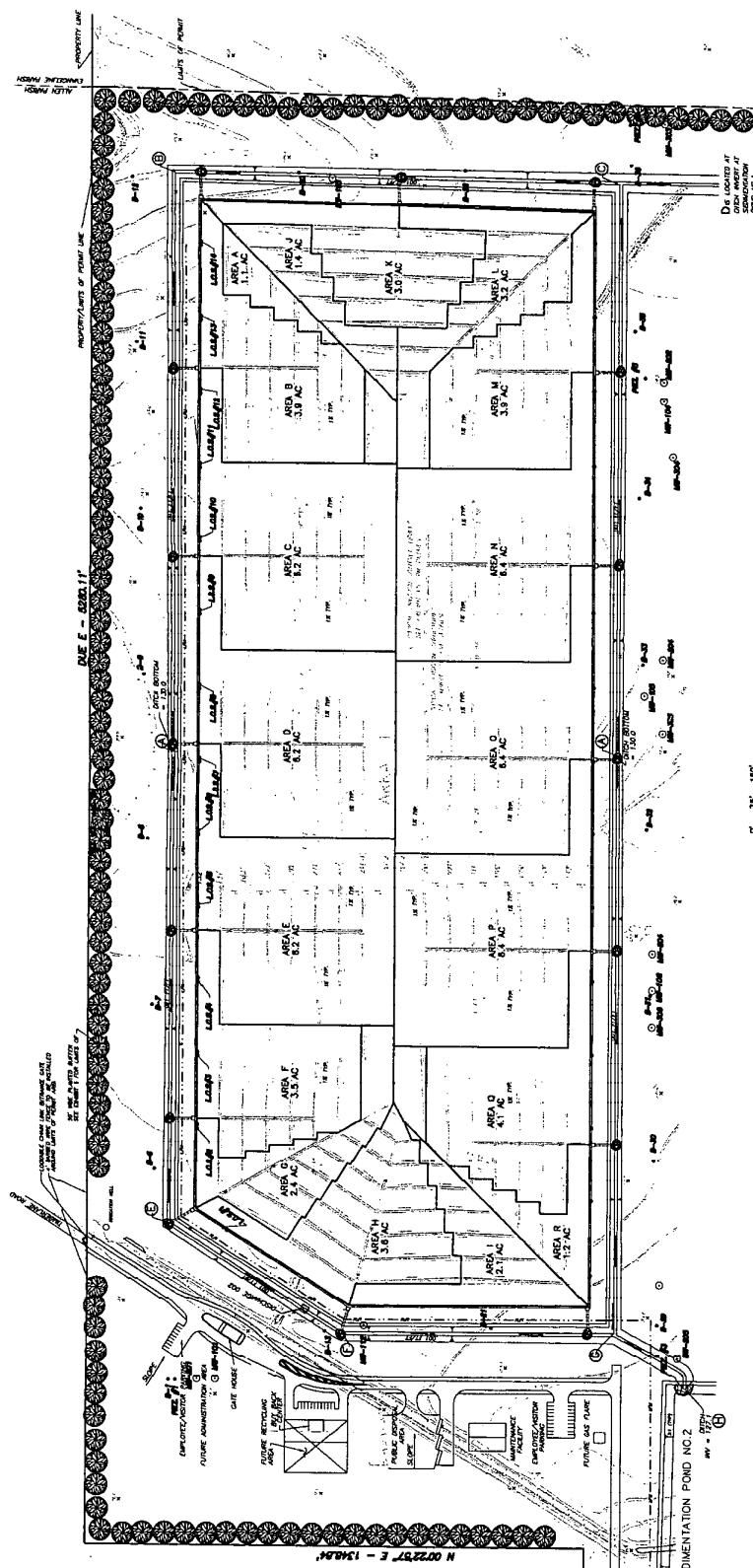










**LEGEND.**

AREA A	Land used or proposed for industrial purposes.
AREA B	Land used for residential purposes.
AREA C	Land used for agricultural purposes.
AREA D	Land used for other purposes.
AREA E	Land used for commercial purposes.
AREA F	Land used for industrial purposes.
AREA G	Land used for residential purposes.
AREA H	Land used for agricultural purposes.
AREA I	Land used for other purposes.
AREA J	Land used for commercial purposes.
AREA K	Land used for industrial purposes.
AREA L	Land used for residential purposes.
AREA M	Land used for agricultural purposes.
AREA N	Land used for other purposes.

**EXHIBIT NUMBER 11 - AREA I
STANDARD OPERATING PERMIT APPLICATION
TUMBLERLANE LANDFILL
IESI LA LANDFILL CORPORATION**

Revised dated 1/2/07 (See Construction Contract Owner)
DRAFT Standard Operating Permit
IESI LA Landfill Corporation, Inc.
1212 New Orleans Avenue, Baton Rouge, Louisiana 70801
Tel: (225) 766-0700, Fax: (225) 766-0725

Date: 8/3/07 Date: 8/3/07 Date: 8/3/07

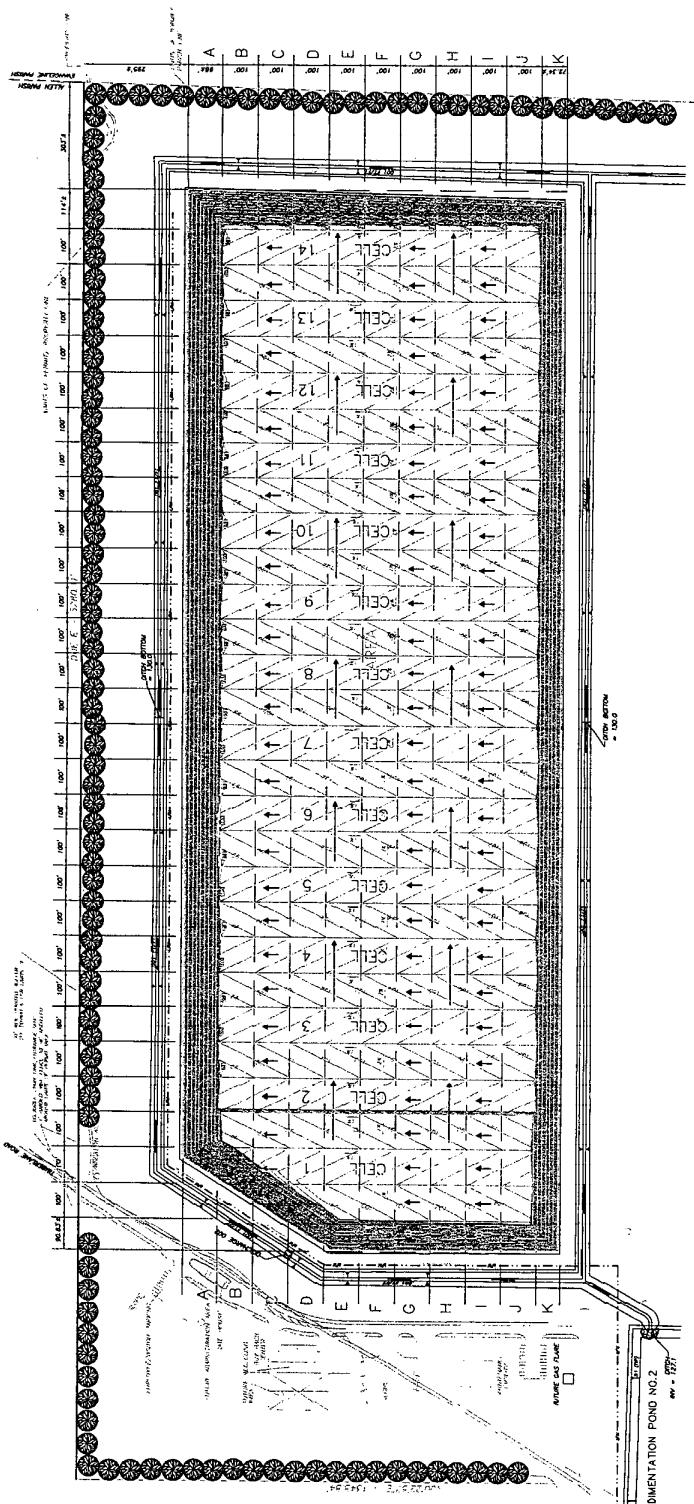
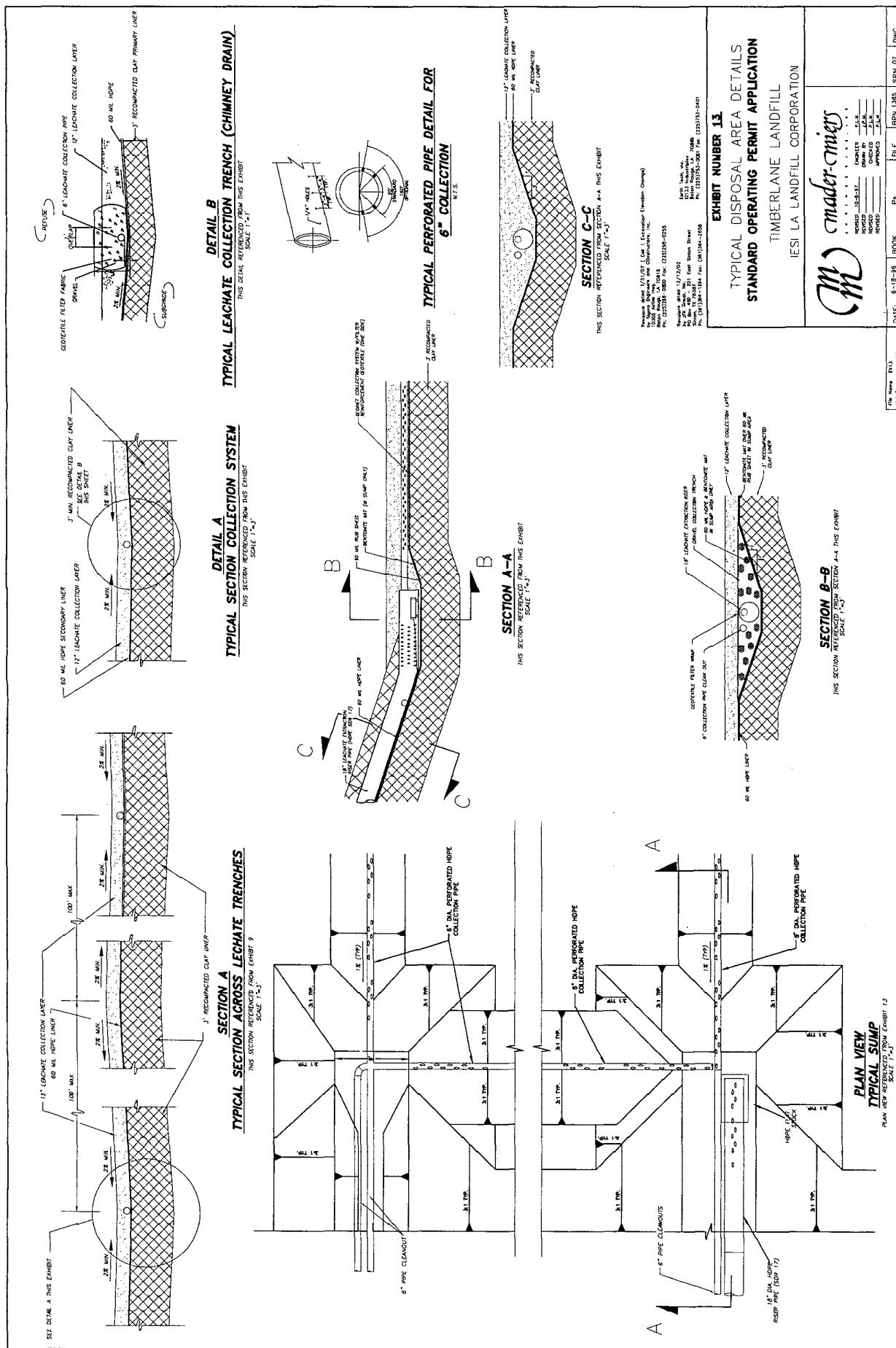
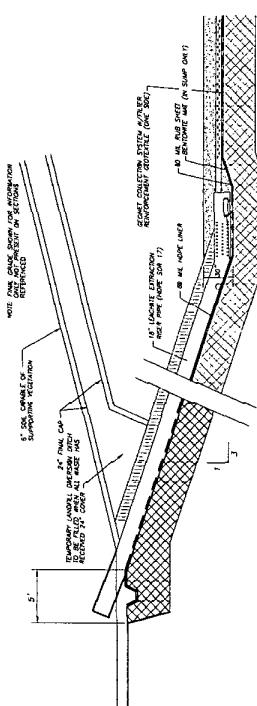


Exhibit Number 12	Site Grid System	Standard Operating Permit Application
Timberlane Landfill	Les La Landfill Corporation	
Proposed Contours	Direction of Flow	Lineation of Fil & Cel.
Cell Number	Sequence of Cell Construction	
Cell 1		
Lines of Property Line		
Lines of Pond		
Cell Lines		

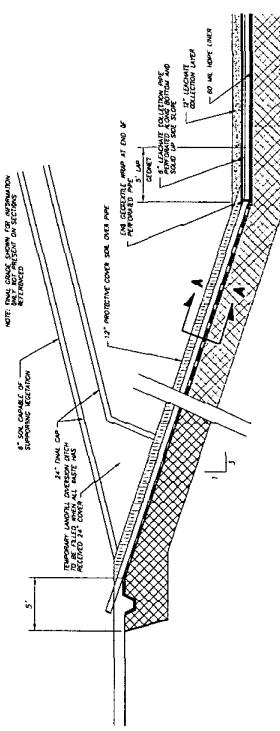




SECTION A
TYPICAL SECTION OF SIDE SLOPE AT COLLECTION SUMP

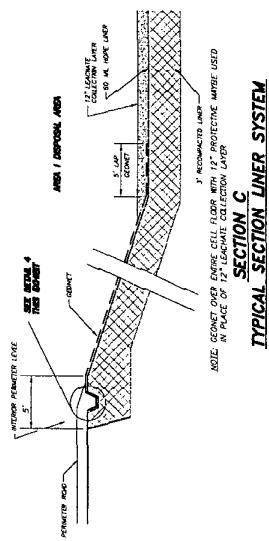
SECTION B
TYPICAL SECTION SIDE LINER AT LEACHATE CLEANOUT PIPE

SECTION REFERRED FROM DRAWINGS 9 & 10



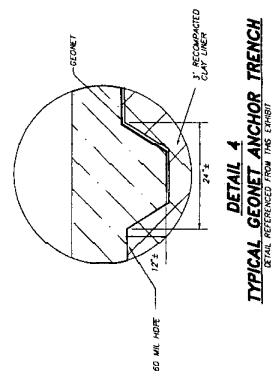
SECTION B
TYPICAL SECTION SIDE LINER AT LEACHATE CLEANOUT PIPE

SECTION REFERRED FROM DRAWINGS 9 & 10



SECTION C
**TYPICAL SECTION LINER SYSTEM
AT SIDE SLOPE**

SECTION REFERRED FROM DRAWINGS 9 & 10



DETAIL 4
TYPICAL GEONET ANCHOR TRENCH

SECTION REFERRED FROM DRAWINGS 9 & 10



SECTION A-A
**TYPICAL LEACHATE CLEANOUT PIPE
ALONG SIDE SLOPE**

SECTION REFERRED FROM DRAWINGS 9 & 10

SECTION REFERRED FROM DRAWINGS 9 & 10

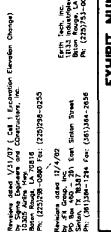
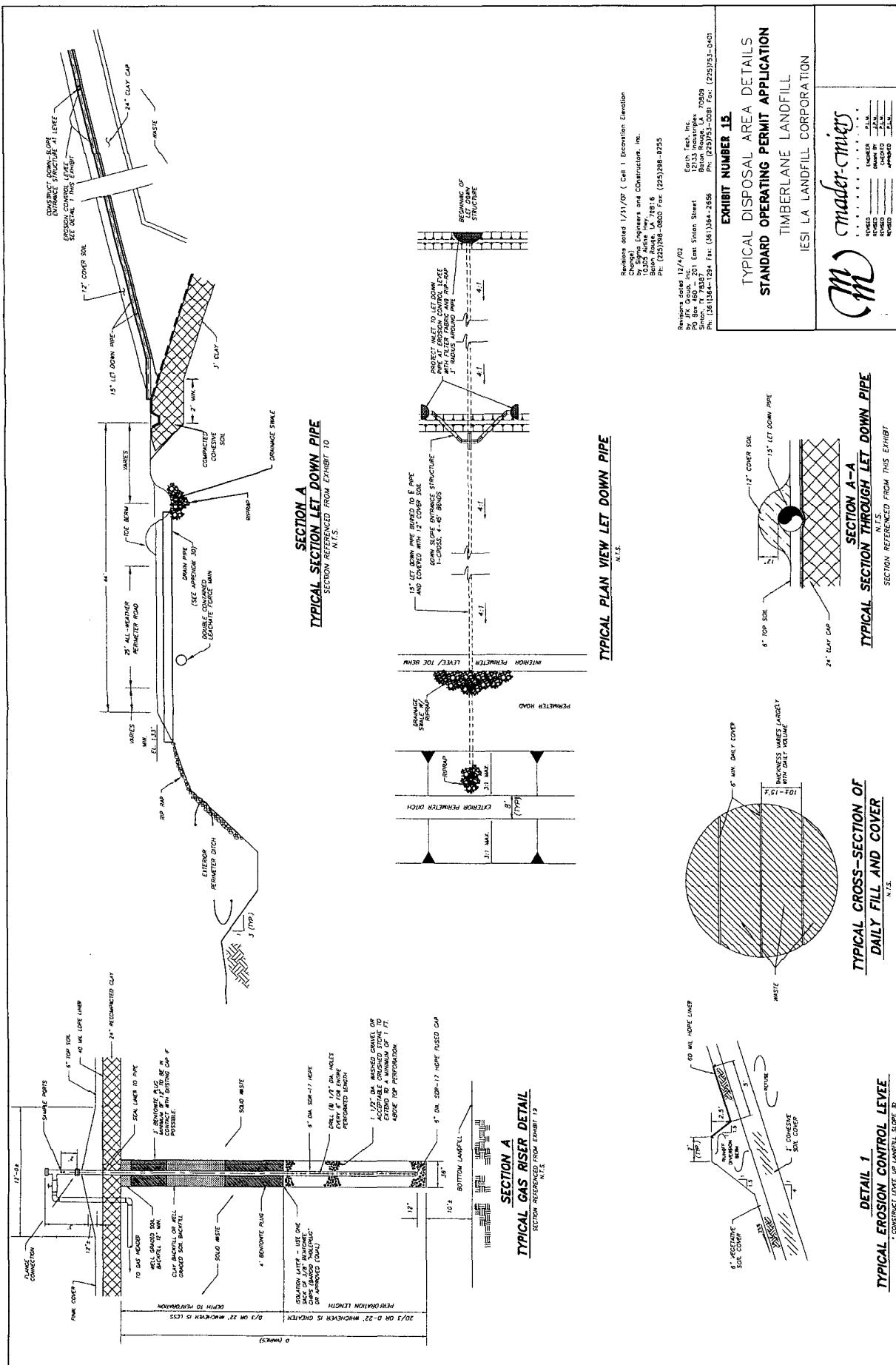


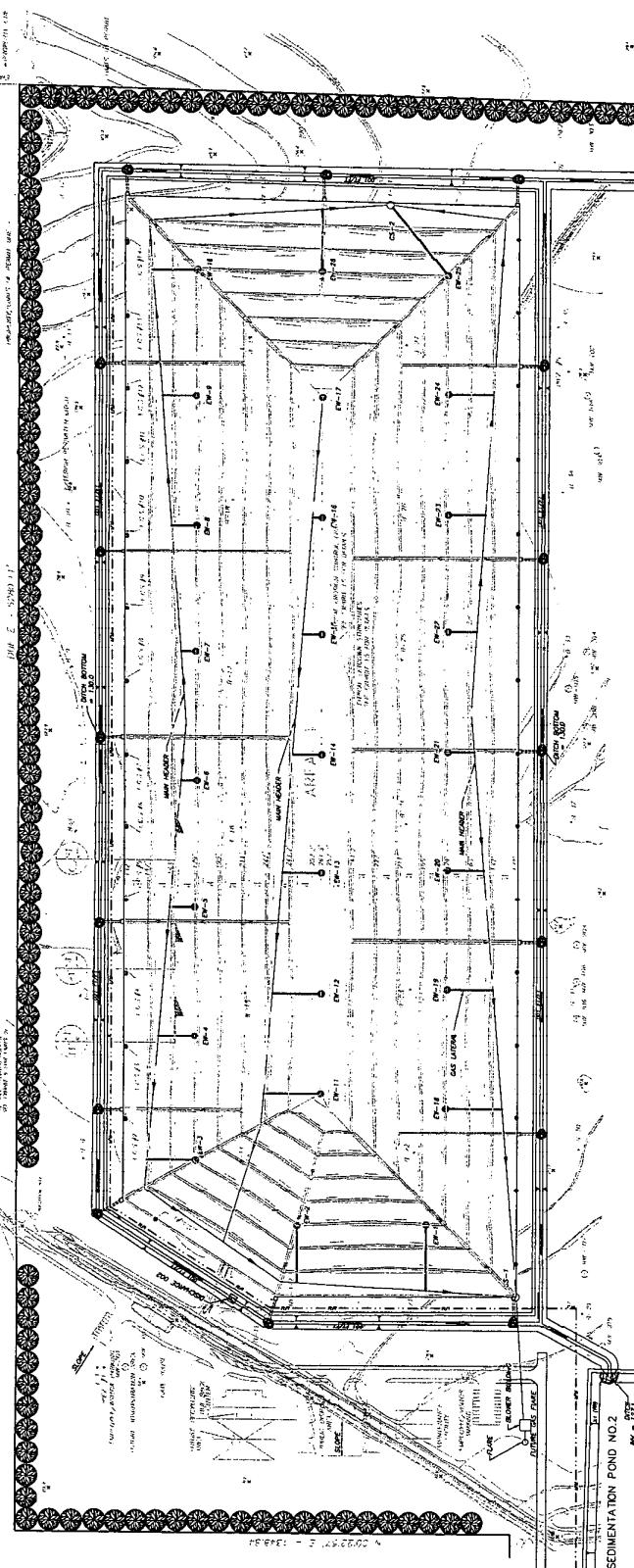
EXHIBIT 14
**TYPICAL DISPOSAL AREA DETAILS
STANDARD OPERATING PERMIT APPLICATION**

TIMBERLANE LANDFILL

IESI LA LANDFILL CORPORATION

Permit Name:	624	Date Issued:	06/24/95	Book:	Pg.	File #:	SPN 285	SPN 27	DMC
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Permit Number 12700 (Landfill Gas Extraction System)
Title: Landfill Gas Extraction System
Permit Type: General
Permit Status: Active
Permit Date: 03/29/2015
Expiry Date: 03/29/2018
Last Renewal Date: 03/29/2015
Last Inspection Date: 03/29/2015
Last Audit Date: 03/29/2015
Last Review Date: 03/29/2015
Last Approval Date: 03/29/2015
Last Denial Date: N/A
Last Rejection Date: N/A

PERMIT NUMBER:	12700
GAS EXTRACTION SYSTEM	
STANDARD OPERATING PERMIT APPLICATION	
TIMBERLINE LANDFILL	
IESI LA LANDFILL CORPORATION	
(M) <i>Timberline Inc.</i>	
DATE ISSUED:	03/29/2015
EXPIRE DATE:	03/29/2018
PERMIT STATUS:	Active
APPROVED BY:	
APPROVING OFFICIAL SIGNATURE:	

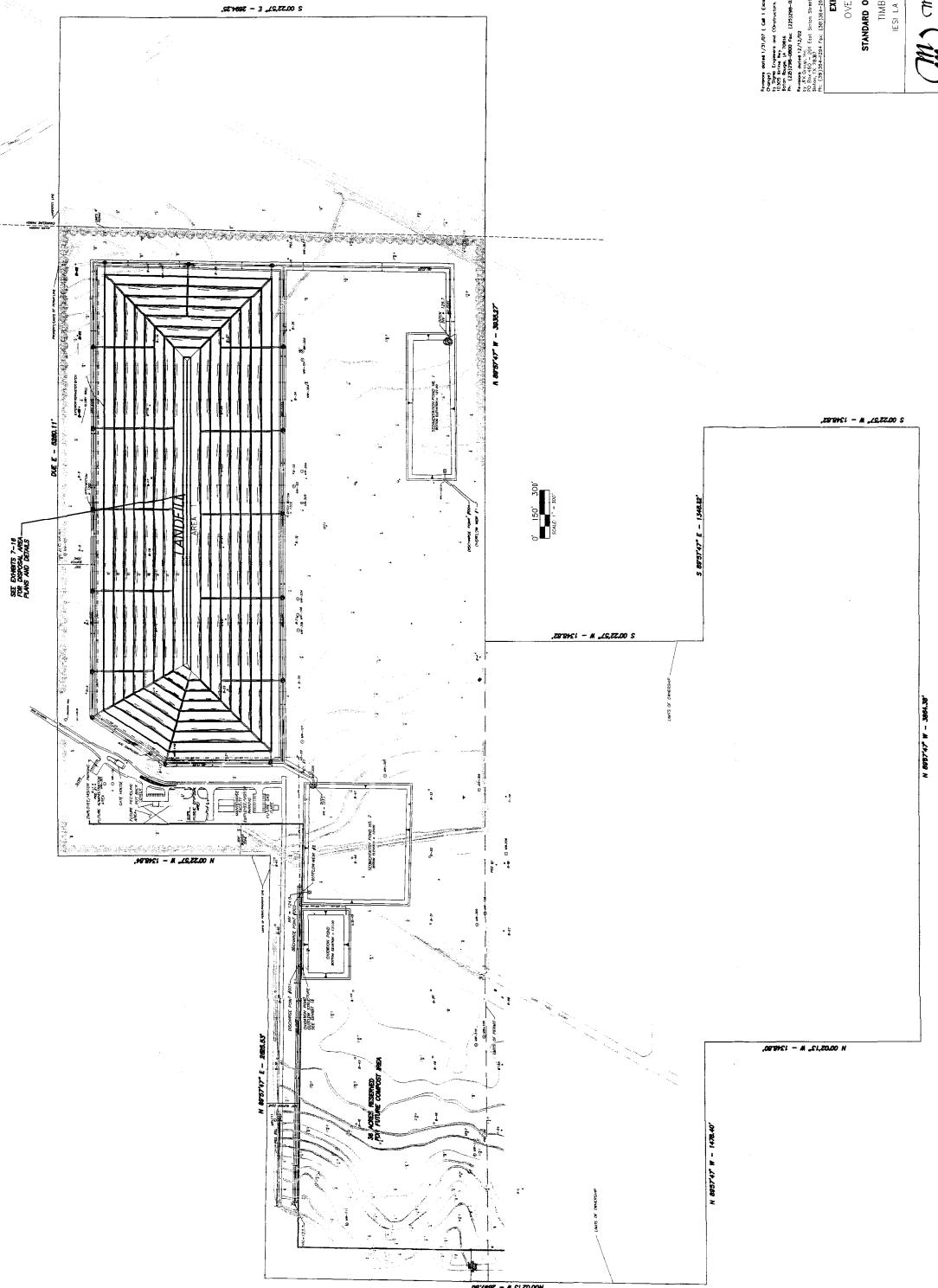
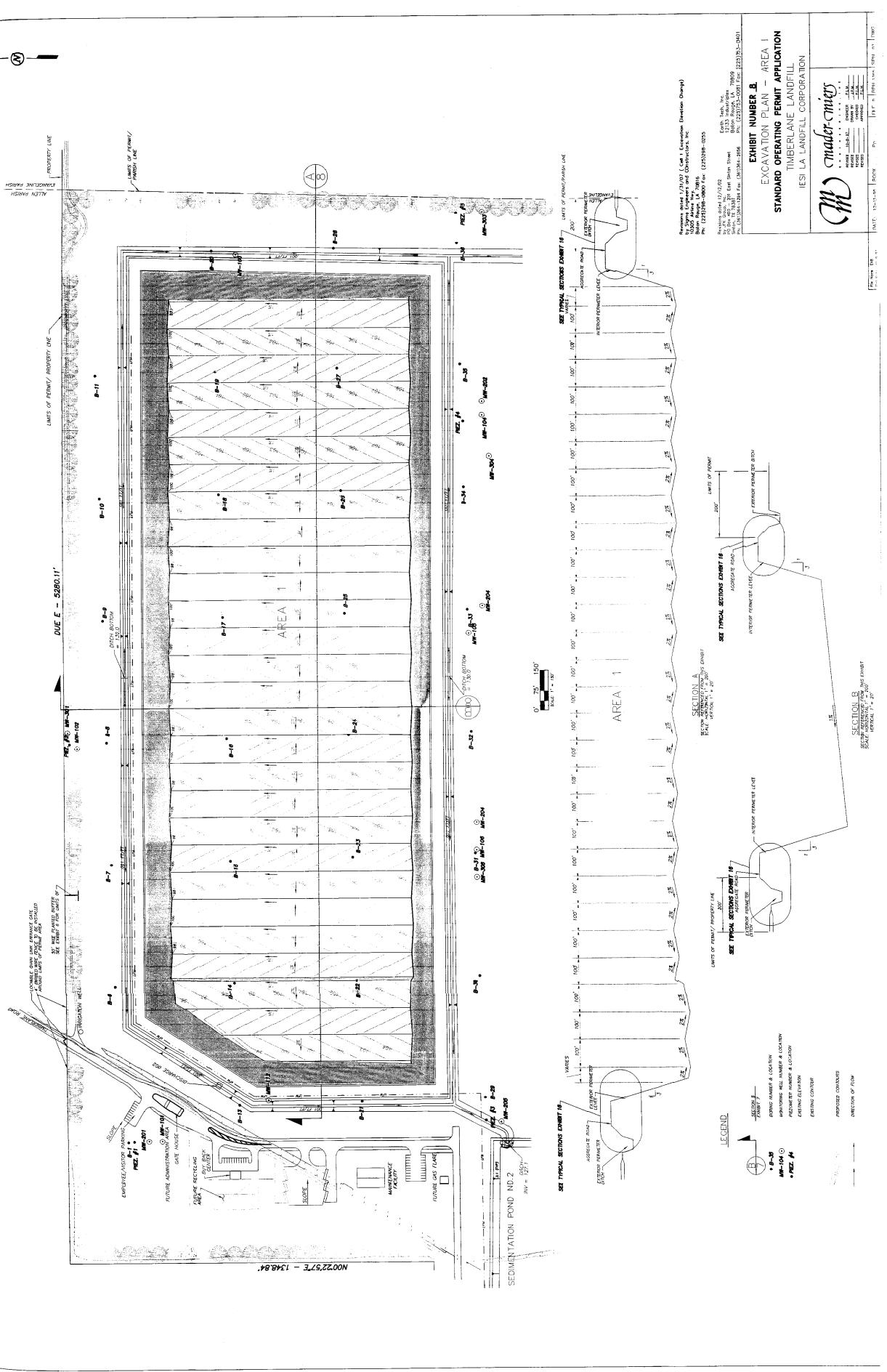
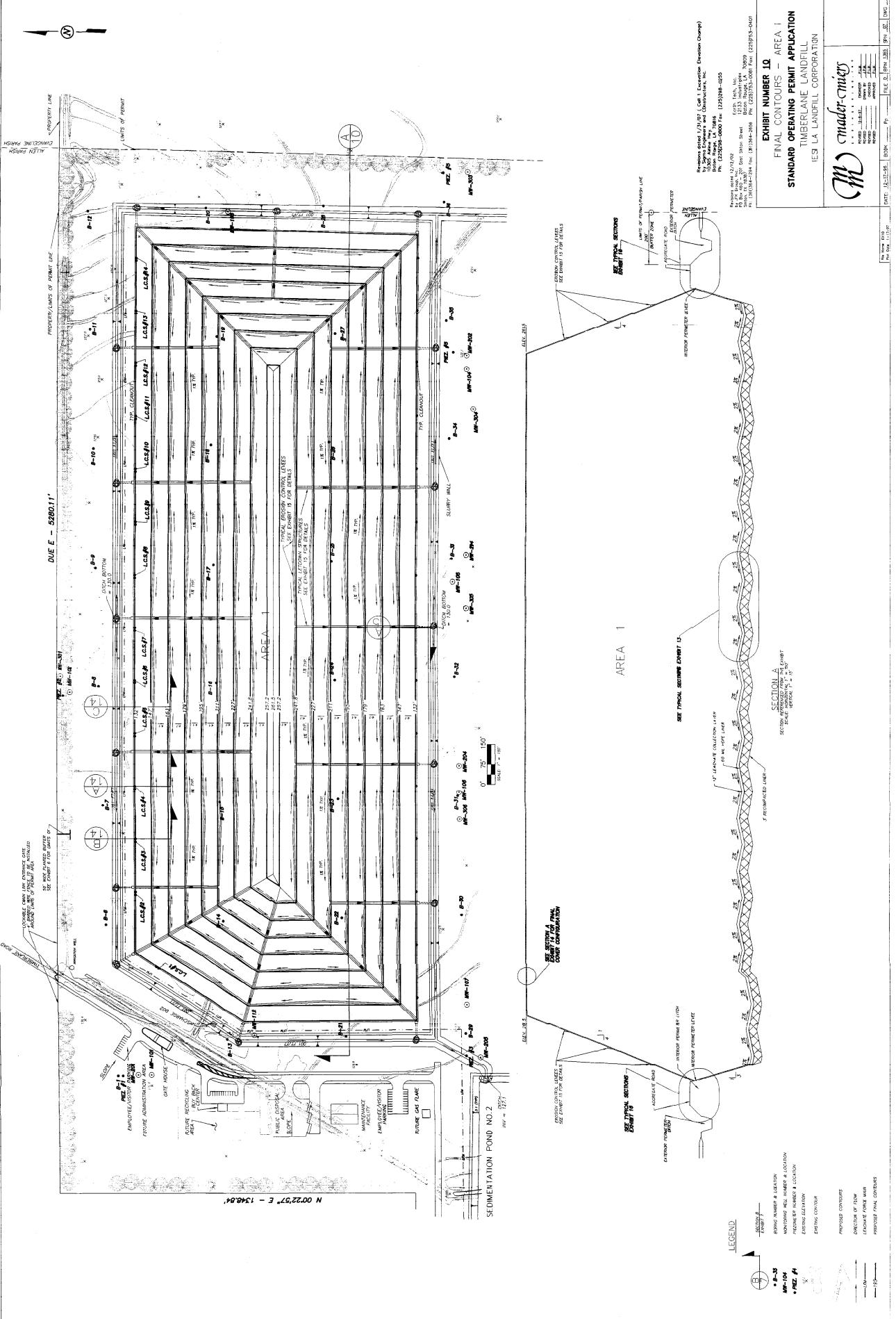
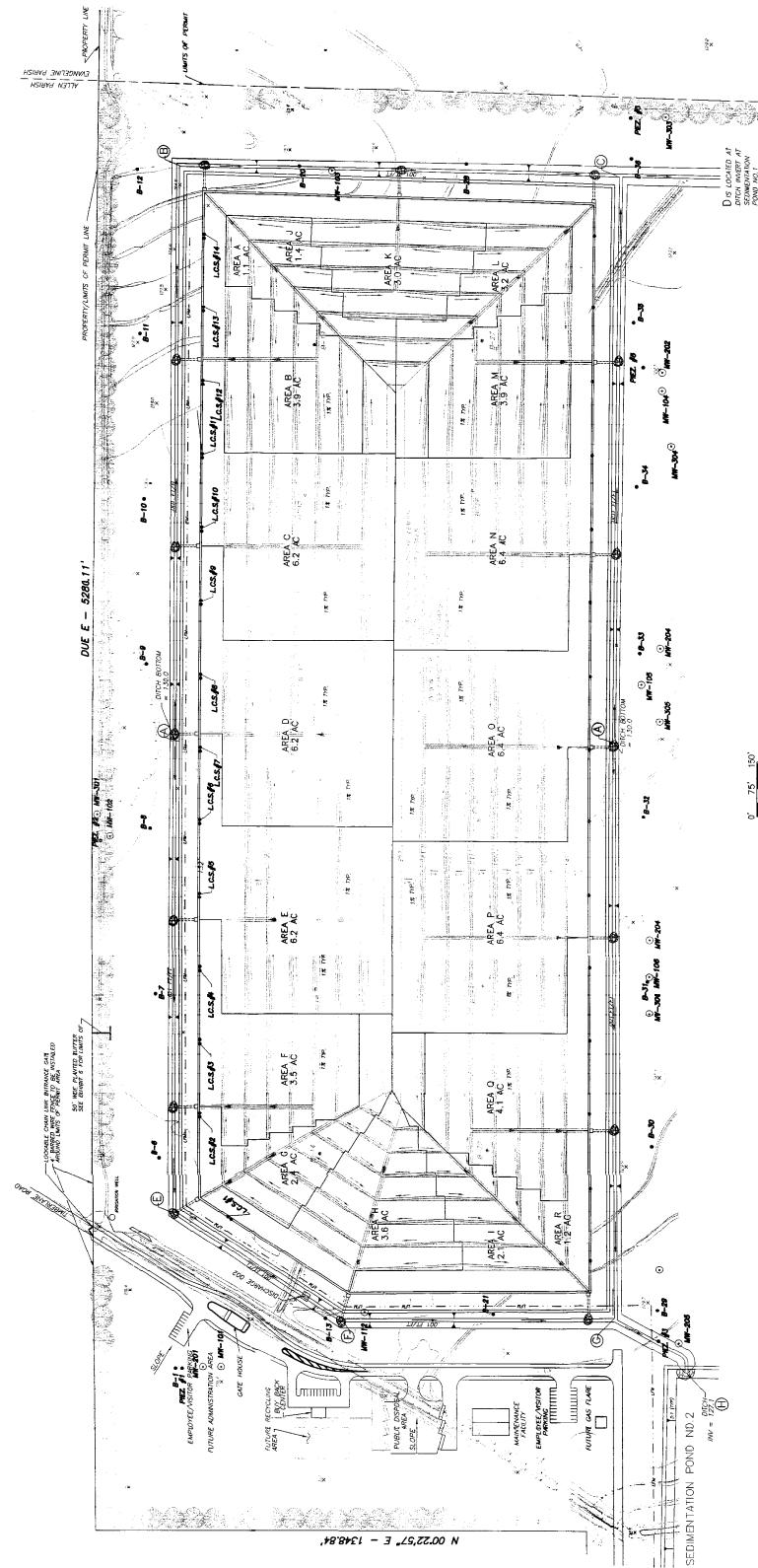


EXHIBIT NUMBER A	
OVERALL SITE PLAN	STANDARD OPERATING PERMIT APPLICATION
TIMBERLINE LANDFILL	LESI LA LANDFILL CORPORATION
<p style="text-align: right;">(M) Under construction</p>	
Ref. No. _____	Ref. No. _____
Date _____	Date _____
Book _____	Book _____
Page _____	Page _____
SN. 100	SN. 100
1W02	1W02







LEGEND



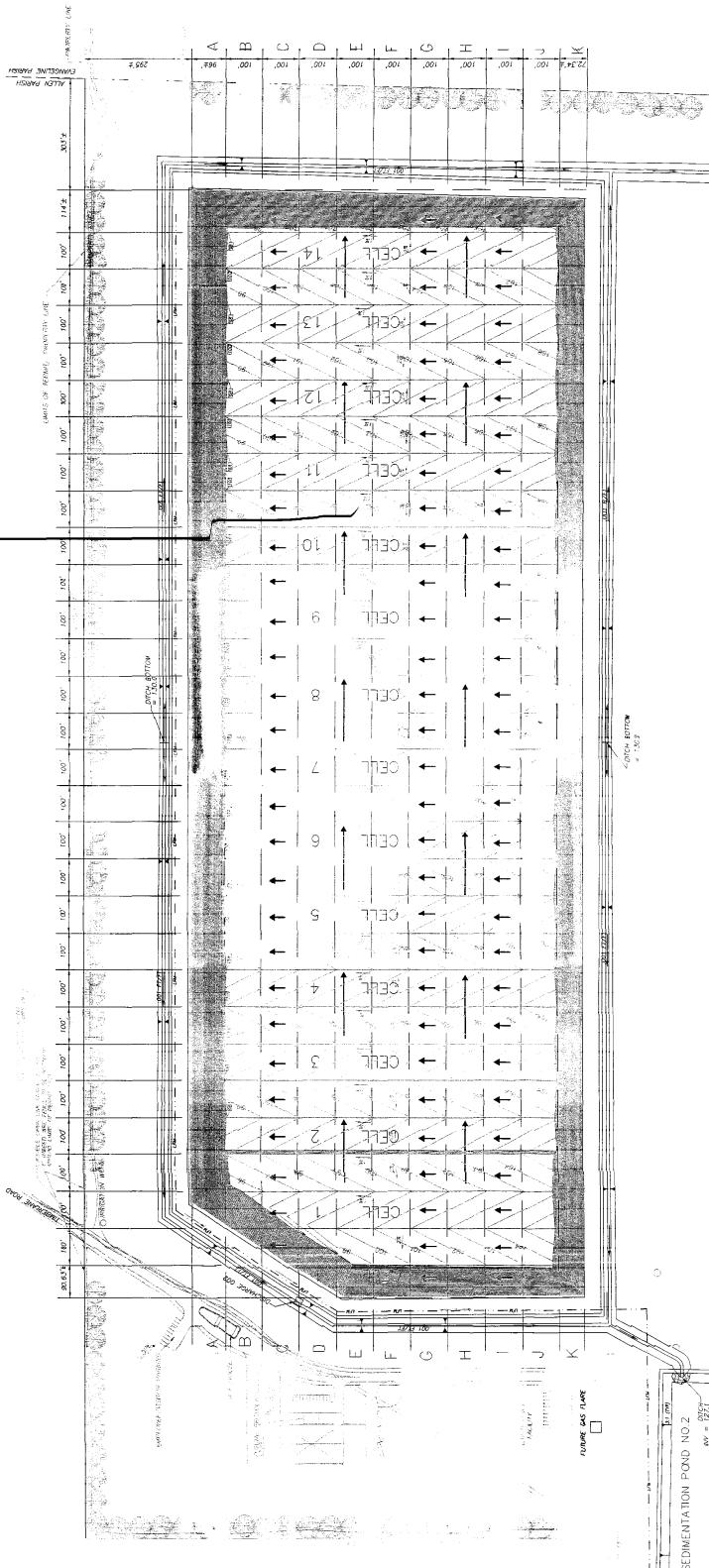
EXHIBIT NUMBER 11
STANDARD OPERATING PERMIT APPLICATION
TIMBERLANE LANDFILL
TELLS LA LANDFILL CORPORATION

(M) *ander-mits*

Permit Number:	529411
Location:	N 33° 45' 30"E, 94° 48' 30"W
Regulatory Number:	E03409
Facility Name:	TIMBERLANE LANDFILL
Facility Type:	Landfill
Facility Address:	P.O. Box 5713, New Orleans, LA 70158-5713
Facility Phone:	(504) 454-2600
Facility Fax:	(504) 454-2610
Fees:	\$1,000
Date Issued:	10/20/97
Term:	02/28/04
Book:	111
Page:	11

Permit Dates Issued: 10/20/97
Expiry Date: 02/28/04
Facility Name: TELL'S LA LANDFILL CORP.
Facility Address: P.O. Box 5713, New Orleans, LA 70158-5713
Facility Phone: (504) 454-2600
Facility Fax: (504) 454-2610
Fees: \$1,000
Date Issued: 10/20/97
Term: 02/28/04
Book: 111
Page: 11

(M) *ander-mits*



LEGEND

- SEQUENCE OF CELL CONSTRUCTION
 - ↑ K SECTION LETTER
 - CELL NUMBER
 - LIMITS OF FILL/PERFIL LINE
 - LIMITS OF FLOOR
 - CELL LINES
- NOTE: AT TIMES DURING THE WASTE PROCESS MORE THAN ONE SECTION OF A CELL OR WASTE ELEMENT TELLS AT THE SAME TIME, SUCH AS CELLS 12 & 3 BEING FILLED SIMULTANEOUSLY STARTING AT THE SAME POINT AND GOING IN OPPOSITE DIRECTIONS. IN THESE CASES, THE PLANNED SEQUENCE LINE LOC'D WILL BE NOTIFIED IN WRITING BY THE PROPOSED CHARTERS.

Engineering Services Co., Inc. • 1000 N. Broad St., Philadelphia, PA 19101
Toll Free: 1-800-343-1000 • Fax: (215) 546-2255

Engineering Office: 672-2222
2000 Peachtree Street, NE
Atlanta, GA 30309
(404) 524-2222 • Fax: (404) 524-2255
Engineering Office: 700-7750
1213 Peachtree Street, NE
Atlanta, GA 30309
(404) 524-7750 • Fax: (404) 524-7755

Engineering Office: 223-2222
2000 Peachtree Street, NE
Atlanta, GA 30309
(404) 524-2233 • Fax: (404) 524-2243

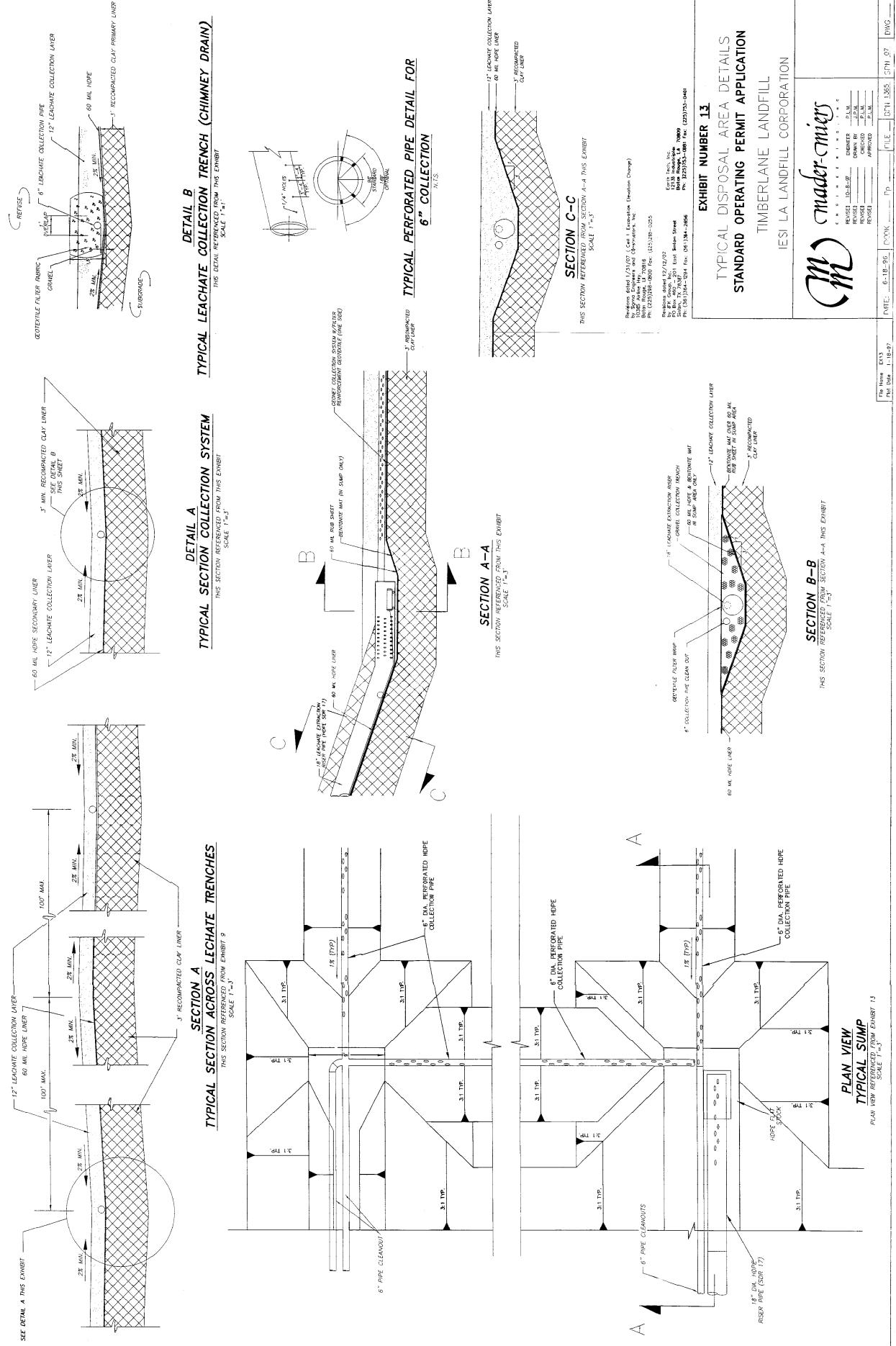
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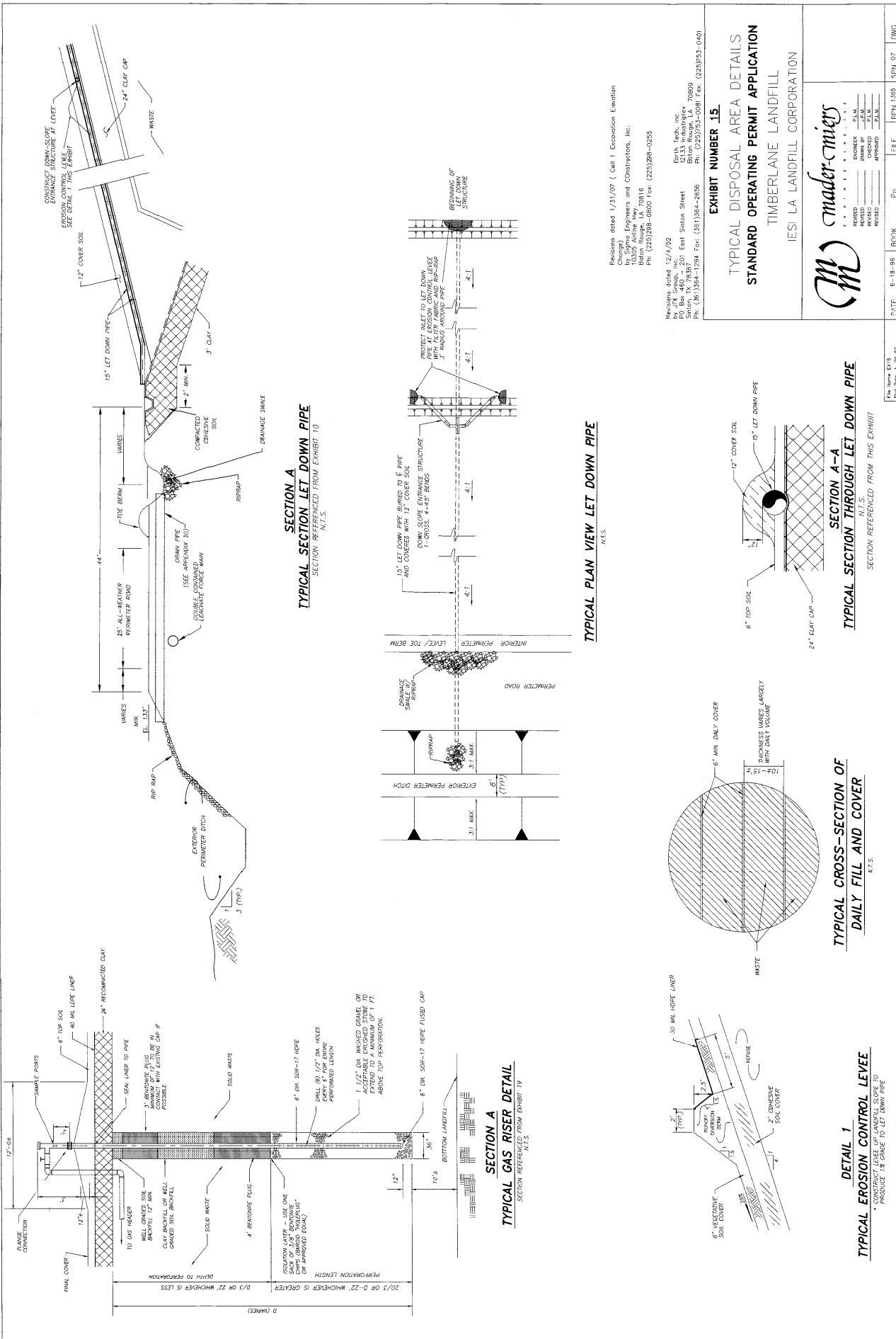
SITE GRID SYSTEM
STANDARD OPERATING PERMIT APPLICATION

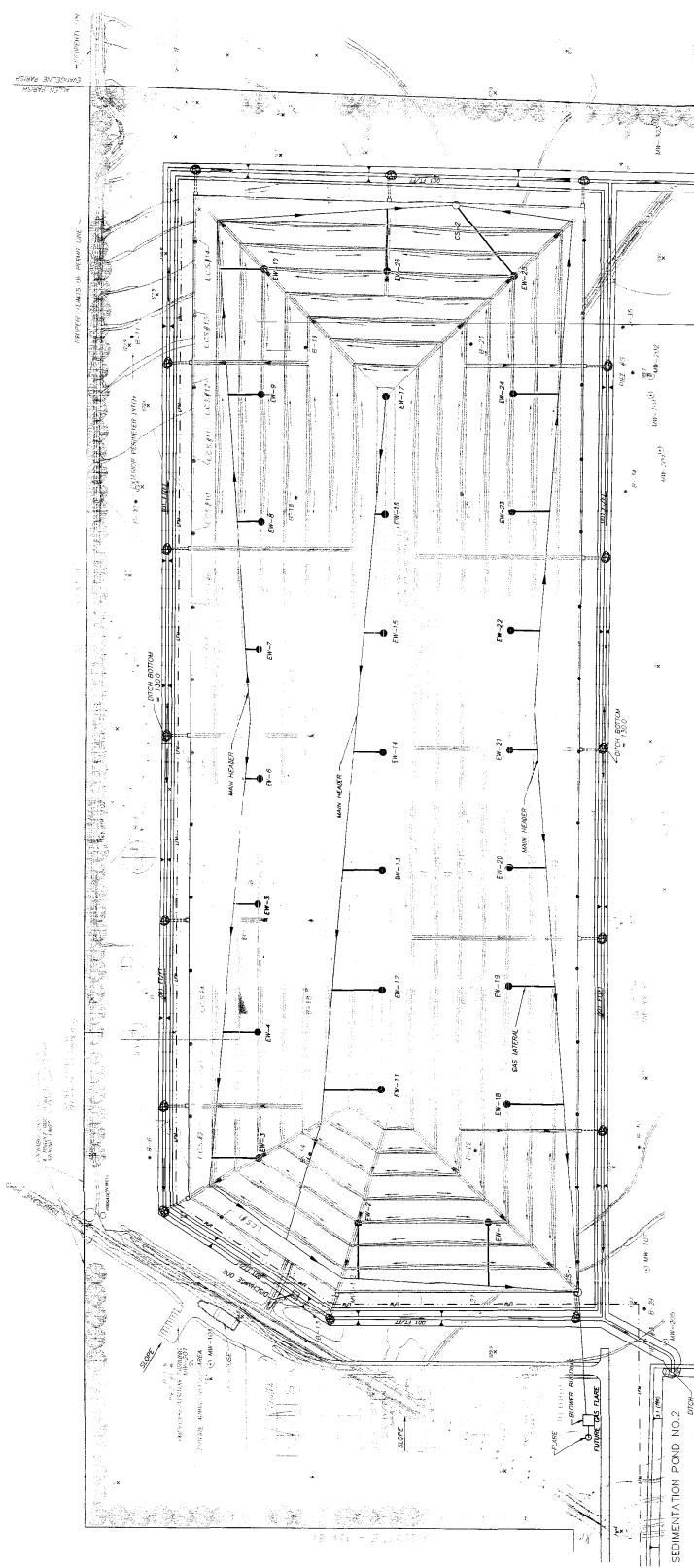
IESI LA LANDFILL CORPORATION



File No. 1000 Rev. 1
File 2. Bem 300 Rev. 1
File 2. Bem 300 Rev. 1







Permit Number 10 of the Gas Extraction System
Gas Extraction System
Timberlane Landfill
ESI LA LANDFILL CORPORATION
Proposed by ESI LA LANDFILL CORPORATION
1320 Timberlane Rd., Suite 100
Metairie, LA 70001
Ph: (504) 837-3400 Fax: (504) 837-3401

EXHIBIT NUMBER 12
GAS EXTRACTION SYSTEM
STANDARD OPERATING PERMIT APPLICATION
TIMBERLANE LANDFILL
ESI LA LANDFILL CORPORATION

(Signature)
Date: 10/22/04
File No.: 101-1225
Page: 1 of 22

LEGEND

- MONITORING WELL & LOCATION
- EXHAUST WELL & LOCATION
- EXISTING CONTOUR
- DIRECTION OF FLOW
- CONVENTIONAL WELL LOCATION AND NUMBER
- GW - GROUNDWATER
- EW - EXHAUST WELL
- EW - EXHAUST WELL LOCATION AND NUMBER

GEOTECHNICAL INVESTIGATION

IESI TIMBERLANE LANDFILL

SIGMA ENGINEERS & CONSTRUCTORS, INC.